

Total marks-234
Very good performance
Keep it up

1(a) Otto cycle,

$$\text{Compression Ratio} = \frac{V_1}{V_2} = r$$

then efficiency of

otto cycle is given by

$$\eta_o = 1 - \frac{1}{r^{\gamma-1}}$$

$\gamma \rightarrow$ ratio of specific heat

let C_v is changed by $p\%$. then New C_v

$$\text{New } C_v \quad C_v' = C_v \cdot p + C_v$$

$$\text{New } C_p \Rightarrow C_p' = C_v' + R \quad [\text{since } R \text{ remains constant}]$$

$$C_p' = C_v p + R + C_v$$

$$\text{new } \gamma' = \frac{C_p'}{C_v'} = \frac{C_v(p+1) + R}{C_v(p+1)}$$

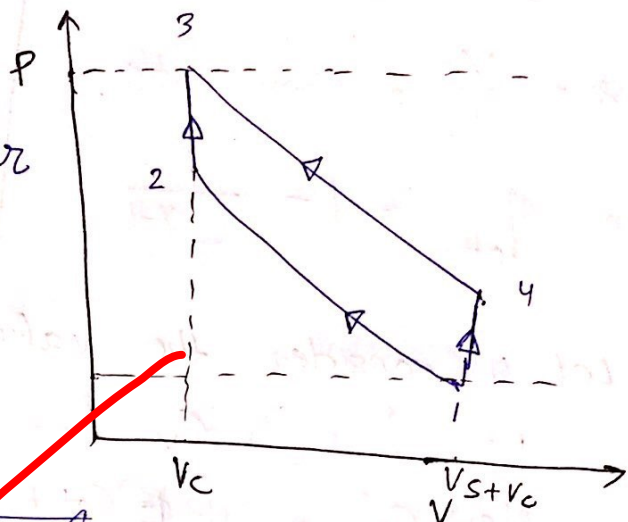
$$= 1 + \frac{R}{C_v(p+1)}$$

$$\gamma' = 1 + \frac{(\gamma-1)}{p+1}$$

$$\gamma' - 1 = \frac{\gamma - 1}{p + 1}$$

$$\gamma' = \frac{p + \gamma}{p + 1}$$

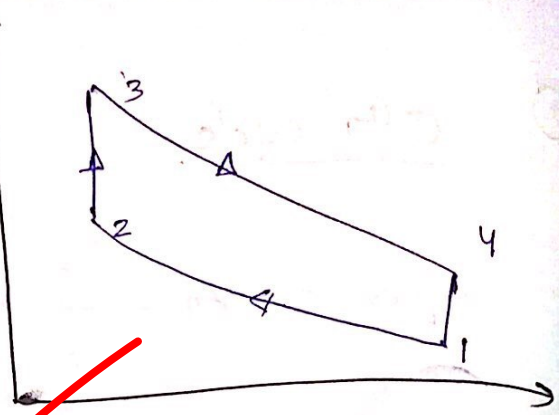
$$\eta_o = 1 - \frac{1}{r^{\left(\frac{\gamma-1}{p+1}\right)}}$$



1(a) Otto Cycle

$$r = \frac{V_1}{V_2} = \text{Comp ratio}$$

$$\text{Then, } \eta_{\text{otto}} = 1 - \frac{1}{r^{\gamma-1}}$$



* Let us consider the value of C_v changes by $p\%$

$$\text{New } C_v' = (1+p)C_v \quad \text{--- (1)}$$

$$\text{New } C_p' = (1+p)C_v + R \quad \text{--- (2)}$$

$$\frac{(2)}{(1)} = \frac{C_p'}{C_v'} = \frac{(1+p)C_v + R}{(1+p)C_v} = 1 + \frac{R}{C_v(1+p)}$$

$$\left(\because \frac{R}{C_v} = \gamma - 1 \right)$$

$$\text{New } \gamma' = 1 + \frac{\gamma - 1}{1+p}$$

$$\boxed{\gamma' - 1 = \frac{\gamma - 1}{1+p}}$$

New Otto cycle efficiency

$$\boxed{\eta_{o,N} = 1 - \frac{1}{(r)^{\frac{\gamma-1}{1+p}}}}$$

$$\% \text{ change in efficiency} = \frac{\eta_{o,N} - \eta_o}{\eta_o} \times 100$$

$$= \frac{\left(1 - \frac{1}{r^{\frac{\gamma-1}{1+p}}} \right) - \left(1 - \frac{1}{r^{\gamma-1}} \right)}{\left(1 - \frac{1}{r^{\gamma-1}} \right)} \times 100$$

$$= \frac{\frac{1}{r^{\gamma-1}} - \frac{1}{r^{\frac{\gamma-1}{1+p}}}}{1 - \frac{1}{r^{\gamma-1}}}$$

Multiplying by z^{Y-1}

$$\frac{1 - z^{Y-1} - \frac{Y-1}{1+p}}{z^{Y-1} - 1}$$

$$\% \text{ change in } \eta = \frac{1 - z^{p(Y-1)}}{z^{Y-1} - 1} \times 100$$

$$p = 0.02, \quad z = 8$$

$$\% \text{ change in } \eta = \frac{1 - 8^{0.02(1.4-1)}}{8^{1.4-1} - 1} \times 100$$

$$= -1.2929\% \quad (\text{decrease by } 1.2929\%)$$

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1(b)

$P_0, T_0, V_0 \Rightarrow$ Pressure, Temp
& velocity of
Atmp air

$P_2, T_2, V_2 \Rightarrow$ " " "
" @ throat area

\rightarrow Assuming air to be
incompressible & inviscid.

App. B.E. b/w 1 & 2.

$$\frac{P_{atm}}{\rho g} + \frac{V_0^2}{2g} + Z = \frac{P_2}{\rho g} + \frac{V_2^2}{2g} + Z$$

$$V_2 = \sqrt{\frac{2(P_{atm} - P_2)}{\rho}}$$

$$(V_2)_{actual} = C_v \sqrt{\frac{2(P_{atm} - P_2)}{\rho}}$$

$$\begin{aligned} \text{mass flow rate of air} &\Rightarrow S_a \cdot \frac{\pi}{4} D^2 \cdot \frac{C_c}{C_d} \cdot C_v \sqrt{\frac{2(P_{atm} - P_2)}{\rho}} \\ &= 1.2 \times \frac{\pi}{4} \times (0.02)^2 \times 0.85 \sqrt{\frac{2 \times 7000}{1.2}} \\ &= 0.0346117 \text{ kg/s} \end{aligned}$$

Similarly mass flow rate of fuel (Neglect lip)

$$\begin{aligned} &= S_f \cdot \frac{\pi}{4} d^2 \cdot C_{df} \sqrt{\frac{2(P_{atm} - P_2)}{\rho_f}} \\ &= 750 \times \frac{\pi}{4} \times (0.00125)^2 \times 0.66 \sqrt{\frac{14000}{750}} \\ &= 2.6245 \times 10^{-3} \text{ kg/s} \end{aligned}$$

$$A/F = \frac{0.0346117}{2.6245 \times 10^{-3}} = \underline{\underline{13.188 \text{ Ans}}}$$

When nozzle lip is considered

max flow rate of fuel

$$m_f = S_f \cdot \frac{\pi}{4} d^2 C_d \sqrt{\frac{\Delta P}{\rho_f}}$$

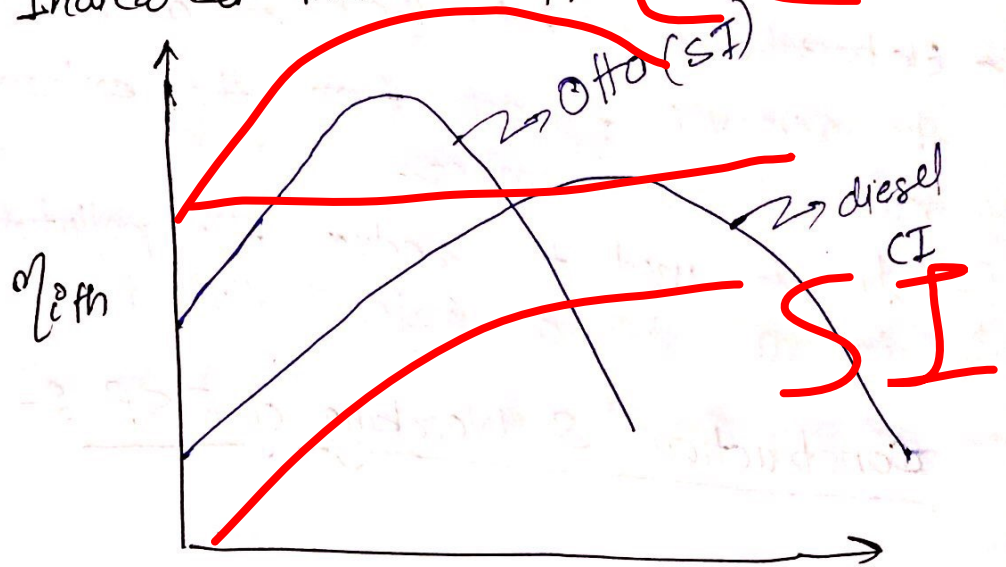
$$= 750 \times \frac{\pi}{4} \times (0.005)^2 \times 0.66 \sqrt{\frac{14000}{750}}$$

Q-1 (C) Methods Improving Performance of Engine

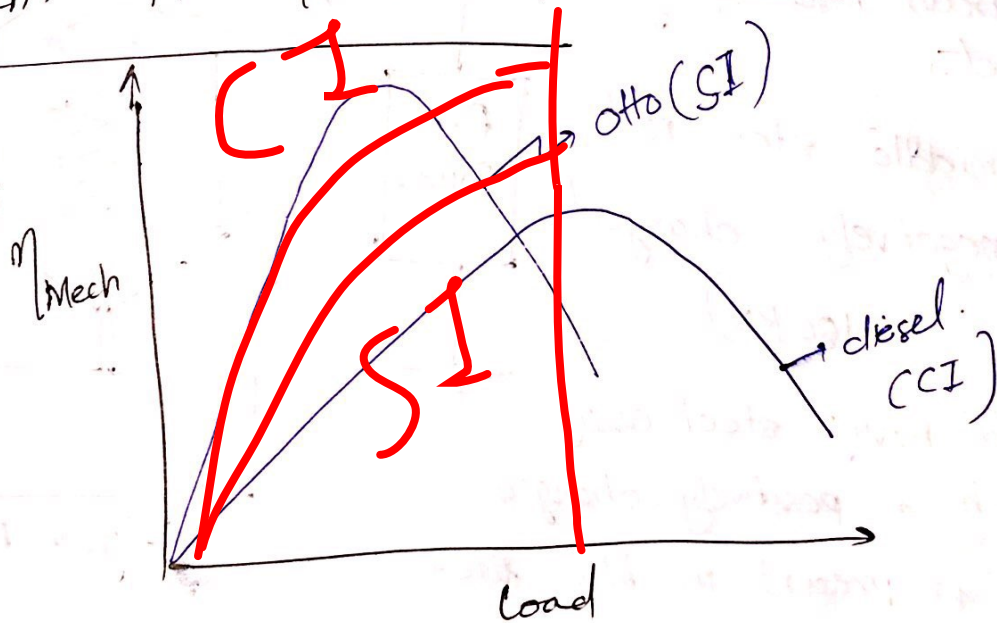
For SI Engine	For CI Engine
* Compression ratio b/w 6-12 but it should be @ lower side to prevent knocking	* Compression ratio should be high 16-22 & should be @ higher side
* Complex fuel structure should be used (Eg: Aromatics & cyclic structure)	* Simple structure are having single bonds Eg: Paraffins
* fuel should have high Ignition delay	* Low Ignition delay fuel should be used.
* For heavy vehicles (high power) Multicylinder engine of small piston is used	* Multicylinder does not preferred hence stroke length should be high
* Supercharging is done to improve specific power	* Turbo charging is done to improve efficiency of the engine.
* TEL & Ethyle dibromide is used.	* Catalytic converter is used to reduce pollution.

Performance Curve for CI & SI Engns

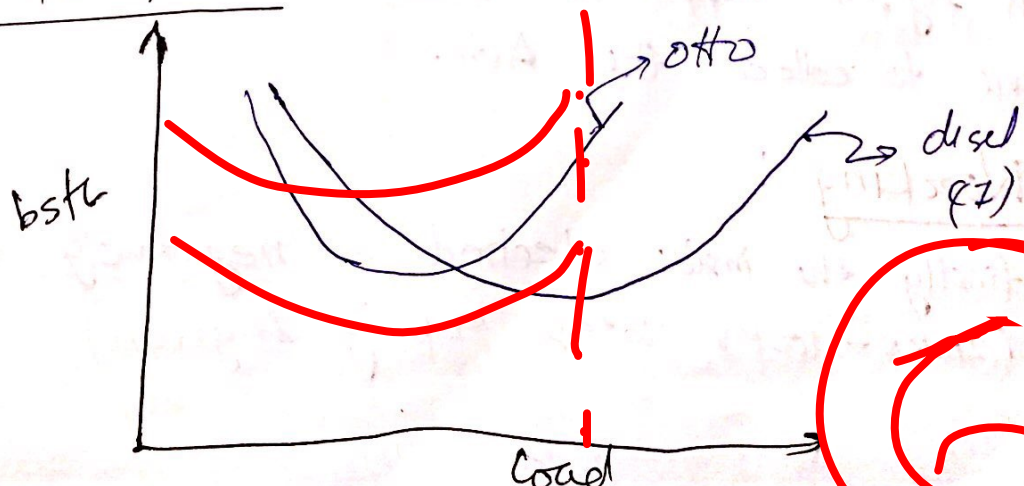
① Variation of Indicated thermal eff with Load



② Mech. eff v/s % Load / % Load



③ bsfc v/s % Load



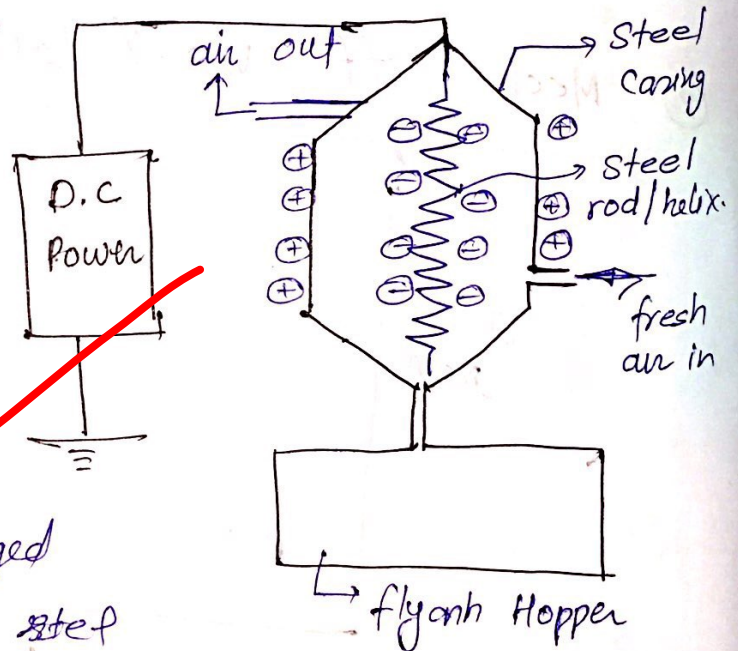
Q-1 (e)

ELECTROSTATIC PRECIPITATOR (ESP)

- Electrostatic precipitator (ESP) is a device used for the removing fly ash from the exhaust of the combustion chamber.
- It is used to reduce the pollution since flyash in air is a major pollutant.

Construction & Working of ESP :-

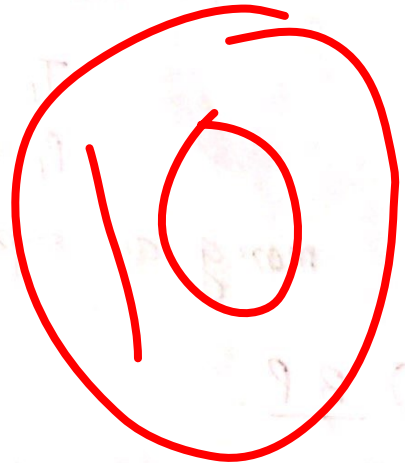
- It consists of 2 Electrodes made up of steel.
- the middle steel rod is negatively charged (40 kV - 100 kV)
- It is having steel casing which is positively charged
- Air is present in b/w steel rods.
- A fly ash hopper is situated below which is used to collect the Ash.



Working :

- firstly, the inside electrode is negatively charged (40 kV - 100 kV voltage supply is given)

- & carrying is charged positively
- due to this high potential difference, the air b/w electrodes gets ionised and dissociates into cation & anion. (positive & negative)
- ~~Positive~~ Negatively charged ion moves towards carrying & it gives charge to fly ash particle when it collides with fly ash.
- fly ash is collected by the plate & Continuous Rammung causes the ash to fall down to fly ash hopper
- This operation is done continuously.



Q-3(a)

$K = 8$ (eight cylinder) four stroke

bore $D = 9 \text{ cm} = 0.09 \text{ m}$

stroke len. $L = 8 \text{ cm} = 0.08 \text{ m}$

Comp. ratio $r_c = 7$

$N = 4500 \text{ rpm}$

arm length $a = 50 \text{ cm} = 0.5 \text{ m}$

Time of Testing $t = 10 \text{ minutes}$

dyn. reading $m = 42 \text{ kg}$

mass of fuel consumed $m_f = 4.4 \text{ kg}$

Calorific value $CV = 44 \text{ MJ/kg}$

$T_1 = 300 \text{ K}$

$P_1 = 1 \text{ bar}$

mass of air supplied $\dot{m}_a = 6 \text{ kg/min}$

① B.P.

(T) Load Torque $= F \cdot a = mg \cdot a$
 $= 42 \times 9.81 \times 0.5$
 $= 206.01 \text{ N.m}$

Brake Power (BP) $= T \cdot \omega = \frac{T \cdot 2\pi N}{60}$

$BP = \frac{2\pi \times 4500}{60} \times 206.01$

$BP = 97.08 \text{ kW}$ Ans

'swept vol^m/sec $= \dot{V}_s = \frac{\pi D^2 L N K}{4 \times 120} = \frac{\pi \times 0.09^2 \times 0.08 \times 8 \times 4500}{4 \times 120}$
 $= 0.15268 \text{ m}^3/\text{s}$

② brake mean eff. pressure $P_{m,b}$

$$BP = P_{b,m} \cdot \dot{V}_s$$

$$97.08 = P_{b,m} \times 0.15268$$

$$P_{b,m} = 635.84 \text{ KPa. An}$$

③ Bsfc \rightarrow mass flow rate of fuel

$$bsfc = \frac{\dot{m}_f}{B.P} = \frac{4.4}{(10 \times 60)(97.08)} = 7.554 \times 10^{-5} \frac{\text{kg}}{\text{KJ}}$$

$$= 0.27194 \frac{\text{kg}}{\text{kwhr.}}$$

④ Brake specific air consumption \therefore (bsac)

$$bsac = \frac{m_a}{BP} = \frac{6}{60 \times \frac{97.08}{3600}}$$

$$bsac = 3.708 \frac{\text{kg}}{\text{kwhr}} \text{ An}$$

⑤ Brake thermal eff.

$$\eta_{b,th} = \frac{BP}{\dot{m}_f \cdot CV} = \frac{97.08}{\frac{4.4}{10 \times 60} \times 44000} = 0.3008$$

$$\eta_{b,th} = 30.08\% \text{ An}$$

⑥ Vol^m eff.

Applying Ideal Gas eqⁿ $P \dot{V}_a = \dot{m}_a R T$

$$100 \times \dot{V}_a = \frac{6}{60} \times 0.287 \times 300$$

$$= 0.861$$

$$\eta_v = \frac{\dot{V}}{\dot{V}_a} = 56.39\% \text{ An}$$

⑦ A/F Ratio

$$= \frac{m_a}{\dot{m}_f} = \frac{6 \times 10}{4.4} = 13.636 \text{ An}$$

Q-3 (b)

$$\text{Swept vol}^m V_s = 3000 \text{ cm}^3$$

$$P_1 \text{ BHP} = 14 \text{ kW/m}^3 \text{ of air/min.}$$

$$\text{volum. eff } \eta_v = 0.85 = \frac{\dot{V}_a}{V_s}$$

$$V_a = 0.85 \times 3000$$

$$V_a = 2550 \text{ cm}^3$$

$$\dot{V}_a = \frac{2550 \times 3500}{1000 \times 2}$$

$$= 4.462500 \times 10^6 \text{ cm}^3/\text{min.}$$

$$= 4.4625 \text{ m}^3/\text{min.}$$

$$\text{BHP}_1 = 14 \times 4.4625 \times 0.8$$

$$\text{BHP}_1 = 62.475 \text{ kW} \times 0.8$$

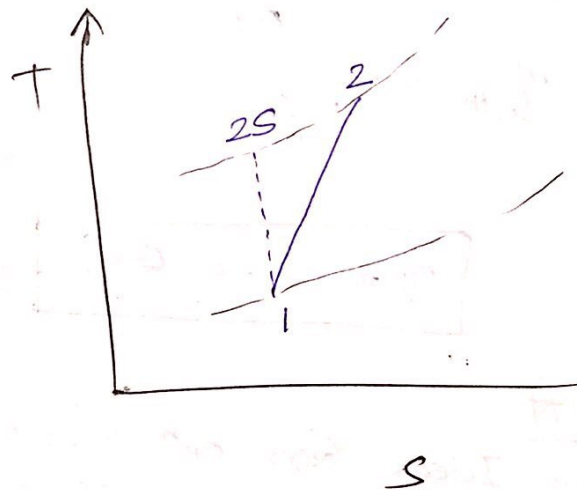
$$\text{BHP}_1 = 49.98 \text{ kW}$$

② After supercharging

$$\begin{aligned} T_{2s} &= T_1 (r)^{\frac{\gamma-1}{\gamma}} \\ &= 300 \times 1.7^{\frac{0.4}{1.4}} \\ &= 349.11 \end{aligned}$$

$$\frac{T_{2s} - T_1}{T_2 - T_1} = 0.8$$

$$T_2 = 361.89$$



Work done by Engne for supercharging

$$\begin{aligned} W &= \dot{m}_a [C_{pa} (T_2 - T_1)] \\ &= \delta V_a [C_{pa} (T_2 - T_1)] \\ &= \frac{P_1}{RT_1} V_a [C_{pa} (T_2 - T_1)] \\ &= \frac{101.03}{0.287 \times 300} \times \frac{4.4625}{60} [1.005 (361.39 - 300)] \\ &= \underline{5.3987 \text{ kW}} \end{aligned}$$

New air flow rate to cyl/min

$$= 3000 \text{ cm}^3 \times \frac{3500}{2}$$

$$= 5.25 \text{ m}^3/\text{min}$$

$$BP_2 = 14 \times 5.25 = 73.5$$

but 5.3987 kW power given to blower

$$\begin{aligned} (BP_2)_{\text{actual}} &= (73.5 - 5.3987) \eta_{\text{mech}} \\ &= \underline{54.48 \text{ kW}} \end{aligned}$$

change in power

$$\begin{aligned} \Delta BP &= BP_2 - BP_1 \\ &= 54.48 - 49.90 \end{aligned}$$

Please refer solution

$$= \underline{4.501 \text{ kW}}$$

Q - 3 (C)

pressure ratio $r_p = 8$

Temp @ entry $T_1 = 300 \text{ K}$
to comp

Temp at entry of Turb $T_3 = 1300 \text{ K}$

isent. eff of comp $\eta_c = 0.8$

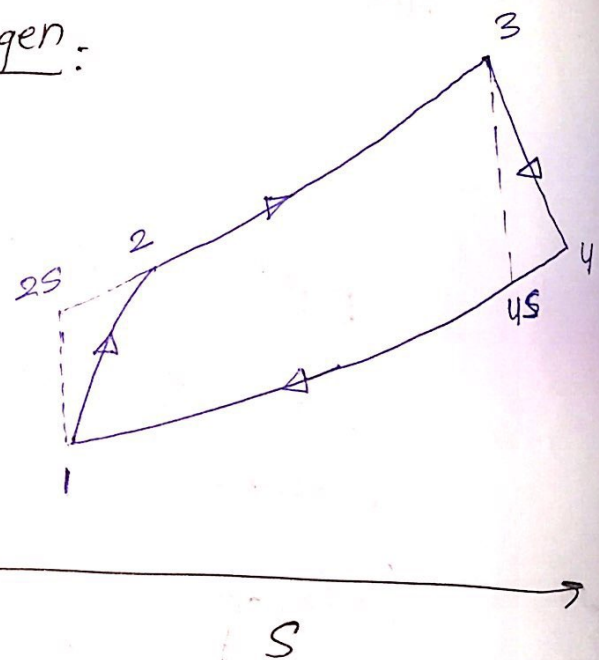
isent eff of Turb $\eta_T = 0.85$

Eff of Regen. $\epsilon = 0.8$

(i) Thermal eff without Regen.

Assump:

1. Air is a working substance
2. Air is assumed to be perfect gas
3. C_p, C_v, γ is constant



$$T_{2s} = T_1 (r_p)^{\frac{\gamma-1}{\gamma}}$$
$$= 300 (8)^{\frac{0.4}{1.4}}$$

$$T_{2s} = 543.434 \text{ K.}$$

$$\eta_c = \frac{T_{2s} - T_1}{T_2 - T_1} \Rightarrow 0.8 = \frac{543.434 - 300}{T_2 - 300}$$

$$T_2 = 604.297 \text{ K}$$

$$T_3 = 1300 \text{ K.}$$

$$T_{us} = \frac{T_3}{r_p^{\frac{y-1}{y}}} = \frac{1300}{(8)^{\frac{0.4}{1.4}}}$$

$$T_{ys} = 717.650 \text{ K}$$

$$\eta_T = \frac{T_3 - T_4}{T_3 - T_{4s}} \Rightarrow 0.85 = \frac{1300 - T_4}{1300 - 717.650} \quad \boxed{T_4 = 805 \text{ K}}$$

$$\eta = \frac{W_{\text{net}}}{Q_{\text{supply}}} = \frac{C_p [T_3 - T_4] - C_p [T_2 - T_1]}{C_p [T_3 - T_2]}$$

$$\eta = \frac{(1300 - 805) - (604.297 - 300)}{(1300 - 604.297)}$$

~~$\eta = 27.41\%$~~

11 When Regeneration.

When T_2 & T_4 will remain
Since T_3 is also same
same, T_1 & T_3

$$G = \frac{C_p [T_1 - T_2]}{C_p [T_4 - T_2]}$$

$$0.0 = \frac{T_a - 604.297}{805 - 604.297}$$

$$0.0 = \frac{14}{805 - 604.297}$$

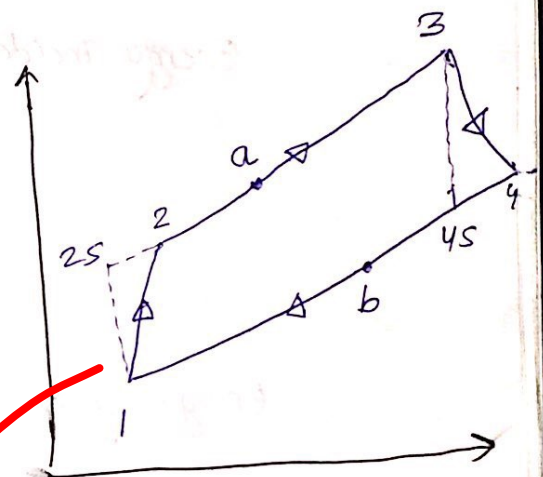
$$= \frac{W_{net}}{Q_s} = \frac{W_T - W_C}{Q_s} = \frac{C_p(1300 - 805) - C_p(604.297 - 300)}{C_p(1300 - 764.86)}$$

$$\eta_g = 35.63\%$$

$$\eta_g = 35.63\%$$

$$\% \text{ change in eff} = \frac{\eta_g - \eta}{\eta} = \frac{35.63 - 27.41}{27.41} \times 100$$

= 29.989% Ans



$$T_g = 764.86 \text{ K}$$

5a)

$$\text{Power O/P of motor} = 2 \text{ hp}$$

$$= 2 \times 746 = 1492 \text{ W}$$

$$\text{motor eff } \eta = 0.85$$

$$\text{Power supplied to motor} = \frac{1492}{0.85}$$

$$= 1755.29 \text{ W}$$

$$\text{cell area} = 140 \times 140 = 19600 \text{ mm}^2$$

$$\text{cell eff } \eta_c = 0.13$$

$$\text{Energy incident on each cell} = H_g \times \text{Area}$$

$$= 1.1 \times 10^3 \times 19600 \times 10^{-6}$$

$$= 81.56 \text{ W}$$

$$\text{Energy given to motor/cell}$$

$$E = 81.56 \eta_c$$

$$E = 2.802 \text{ W/cell}$$

$$\text{Total no of cells req (n)}$$

$$n \cdot E = \text{Power supp to motor}$$

$$n \times 2.802 = 1755.29$$

$$n = 626.26 \text{ cells}$$

$$n = 627 \text{ cells}$$

$$\text{No. of modules Req} = \frac{627}{40} = 15.65 = 16 \text{ modules are required.}$$

Advantages of PV cells

- ① they use the waste solar energy to produce high Grade energy (electricity).
- ② they have low running & Maintenance cost.
- ③ They use renewable energy ~~that~~ & does not produce pollution & noise.
- ④ No Turbines ~~that~~ boiler type heavy & moving part for production of electricity.

10

5b) Grinding wheel

1. A - 70 - K - 7 - V → bond.

↓ ↓ ↓ ↓

Abrasive Grain hardness structure

Grain

Grit

A → Aluminium Oxide (Abrasive)

70 → It denote Grain ~~Grain~~ Grit size

medium Grain size. (in b/w coarse & fine)

K → It belongs to category [I - P]

hardness in Medium

7 → [0 - 7] dense structure [are to finishing]

V → Vitrified bond wheel.

② C - 36 - D - 9 - S - 28

C → Ceramics in the abrasives

36 → medium size Grains is present

D → [A-H] category → SOFT WHEEL

9 → open structure

S → Silicate bond (water Glom)

③ D - 250 - Z - 1 - R

D → Diamond is used as Abrasive

250 - very fine Grains of Abrasive

Z - very hard wheel is used.

1 - dense structure

R → Rubber bond b/w wheel & Abrasive

⑤ ~~Vulcanization of Rubber~~

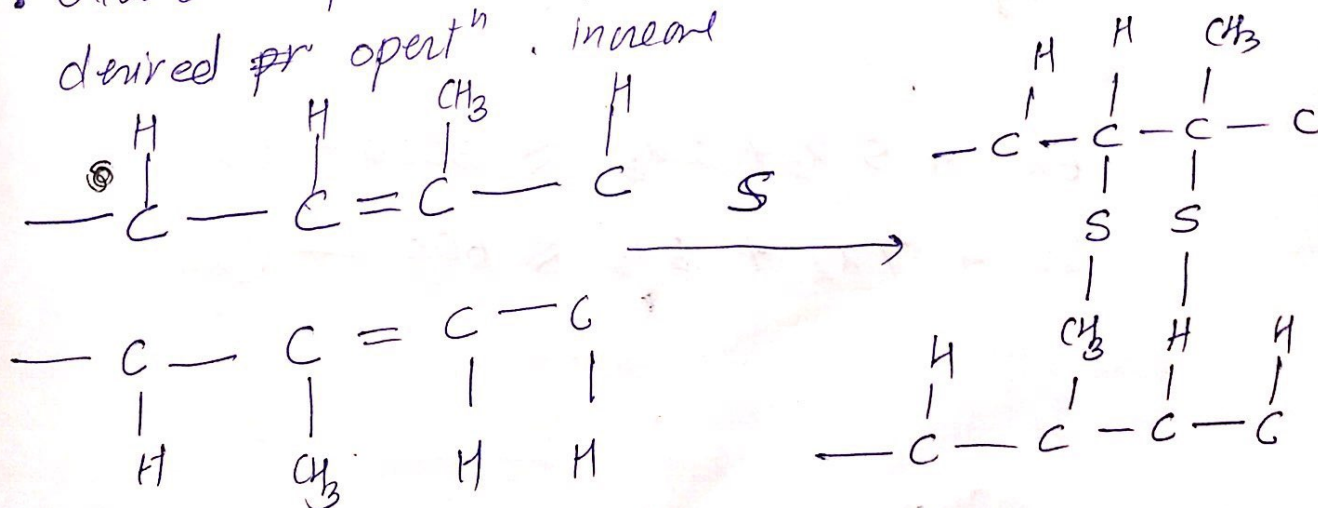
• ~~Vulcanisation is Crosslinking of the polymer~~

5 ©

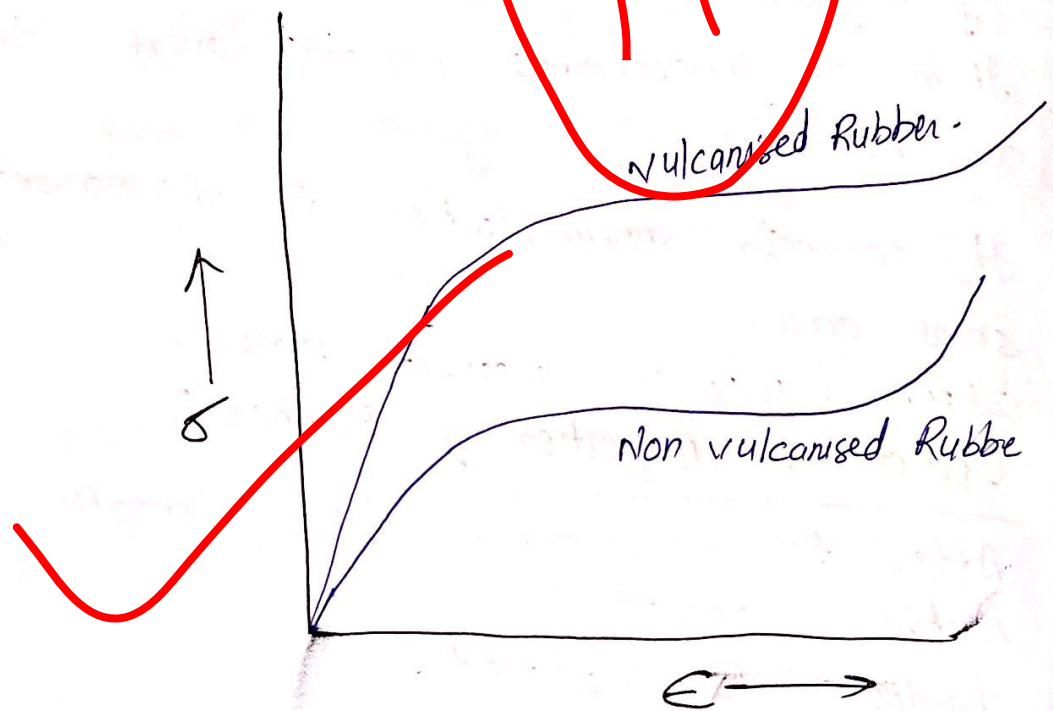
Vulcanization of Rubber

- It is the process of Crosslinking b/w the chain of polymers
 - It is an irreversible process since decrosslinking can not be done again
 - It converts thermoplastic to thermosetting in some cases
 - Sulphur is used in vulcanisation process.
- Effect on Properties of Rubber:-

- After the vulcanisation the strength of the rubber increased
- hardness also increased.
- Vulcanised rubber can withstand at more temperature compared to that of non-vulcanised
- Fatigue & ultimate tensile strength increases
- Increases the cost of rubber due to processing on it
- Overall operational life of component, as per desired μ or σ increases



Stress strain Curve for ~~Vulcanised~~ & Non Vulcanised Rubber



5 (d)

Let

x_1 — No of product A produced

x_2 — " " B "

x_3 — " " C "

$$6x_1 + 5x_2 + 2x_3 \leq 5000 \text{ --- (1)}$$

$$4x_1 + 7x_2 + 3x_3 \leq 6000 \text{ --- (2)}$$

Let time for A = $6t$

Let time to produce A = $6t$

then " " B = $3t$

then " " C = $2t$

Total Time

$$6tx_1 + 3tx_2 + 2tx_3 \leq 1600 \times 6t$$

$$6x_1 + 3x_2 + 2x_3 \leq 9600 \text{ --- (3)}$$

$$x_1 \leq 300 \text{ --- (4)}$$

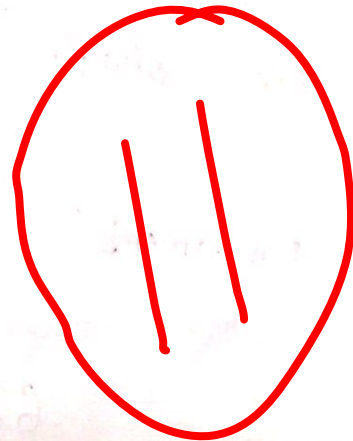
$$x_2 \leq 250 \text{ --- (5)}$$

$$x_3 \leq 200 \text{ --- (6)}$$

$$\frac{x_1}{3} = \frac{x_2}{4} = \frac{x_3}{5}$$

$$Z_{\max} = 90x_1 + 40x_2 + 30x_3$$

These ~~eqⁿ~~ eq^s can be computed out using software @ Program.



5 (e)

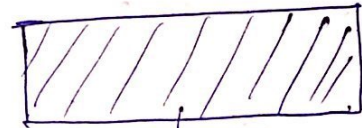
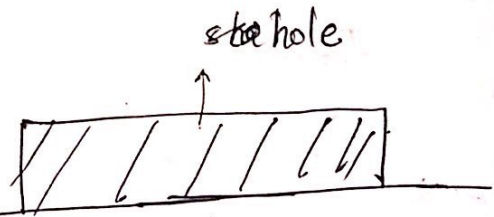
Hole Basis syst

65 H8 f7

$$D = \sqrt{D_1 D_2}$$

$$= \sqrt{50 \times 80} = 63.245$$

basis



shaft

For shaft Tolerance

H8. IT8 is used

$$i = 0.45 \sqrt[3]{D} + 0.001 D$$

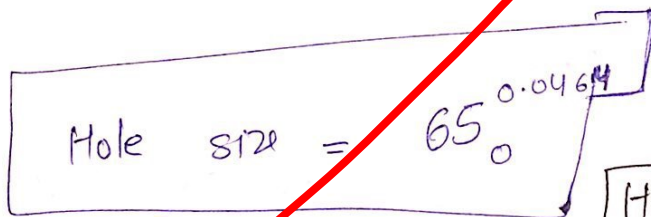
$$= 0.45 \sqrt[3]{63.245} + 0.001 \times 63.245$$

$$= 1.8561 \mu m$$

$$\text{Hole Tolerance} = 25 i = 25 \times 1.8561$$

$$= 46.403 \mu m$$

$$= 0.0464 \text{ mm}$$



fundamental deviation for hole = 0

$$\text{for shaft upper deviation} = -5.5 (63.245)^{0.41}$$

$$= -30.11 \mu m$$

$$= -0.03011 \text{ mm}$$

$$\text{Fundamental deviation of shaft} = -0.03011 \text{ mm}$$

$$\text{shaft Tolerance} = 16 i = 0.02969 \text{ mm}$$

$$65_{-0.03011}^{-0.0598}$$

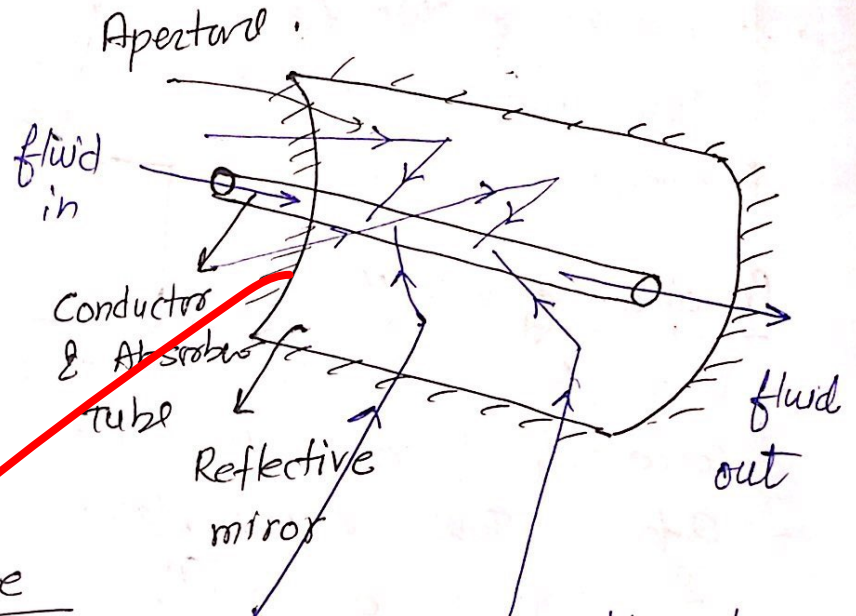
Q-6(a)

1. Cylindrical parabolic concentrator

Construction:

① Reflecting Mirror

It consists a parabolical shaped mirror which is used to reflect the Radiation incident on it.



② Absorber Tube

It is having low diameter, hence concentration of energy is higher & losses are less.

Principle of Working:

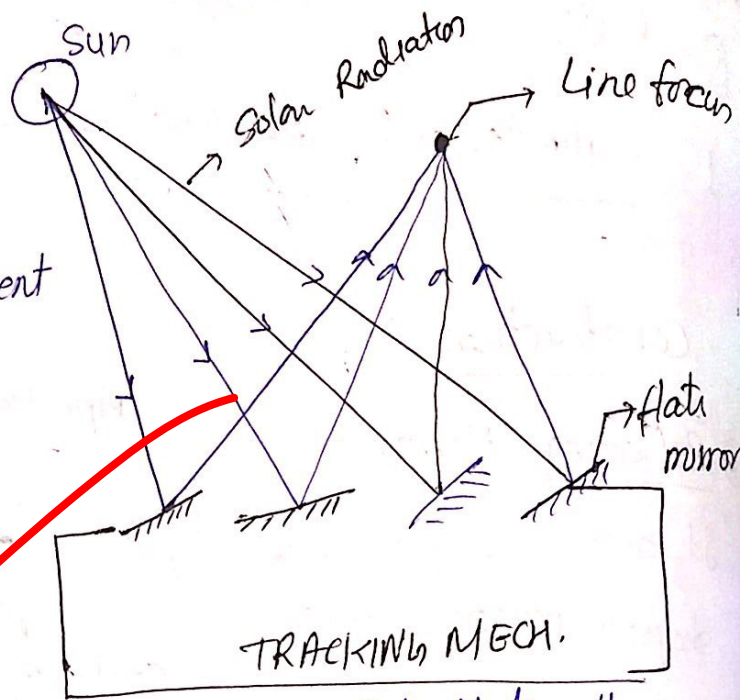
- Thermal Radiation incident on the cylindrical parabolic dish from Random direction.
- due to the property of parabola ~~the~~ Geometry, the Total incident Radiation is focused on a tube carrying water.
- this heat is absorbed by blackened surface & transfer to the heating fluid.

② Linear Fresnel Lens collector :-

It consists of flat mirror which used to concentrate the solar Radiation incident on it

Construction

- It consists of series of flat mirrors ~~that~~ on which the Sun Radiation incident
- It consists of ~~the~~ a Tube line on which the Radiation concentrate



Principle of working

- When ~~Solar~~ Radiation Incident on the flat plate, they concentrate it onto the line of tubing
- Surface of Tubes are blackened & Absorb Radiation & Transfer to the Liquid.

③ Central Tower Receiver

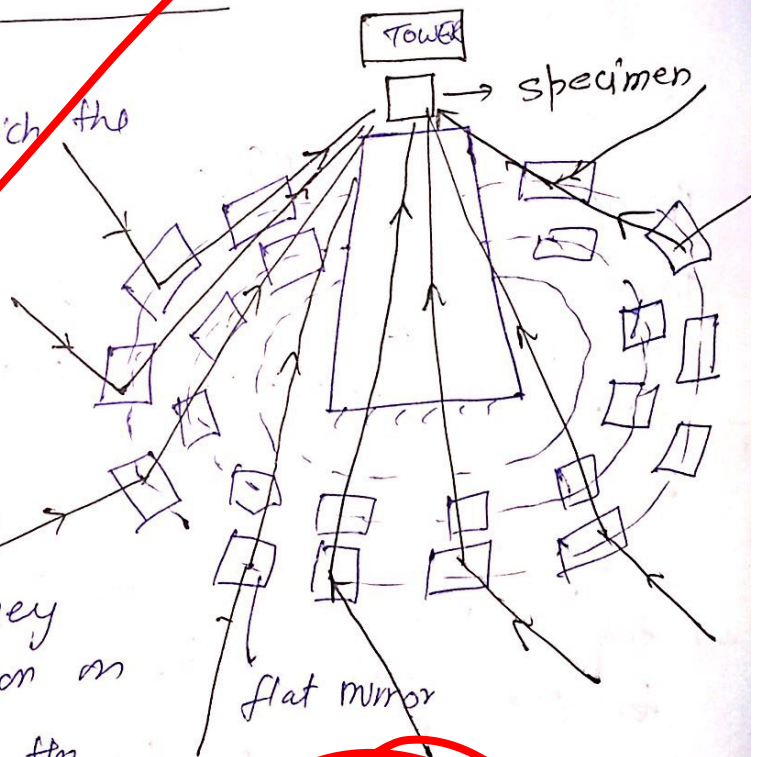
Construction

- Central Tower on which the Solar Rad. is concentrated
- Reflective mirrors
- specimen

Principle of working

Solar Radiation incident on the flat mirrors. they concentrate the Radiation on Central Tower to heat the specimen.

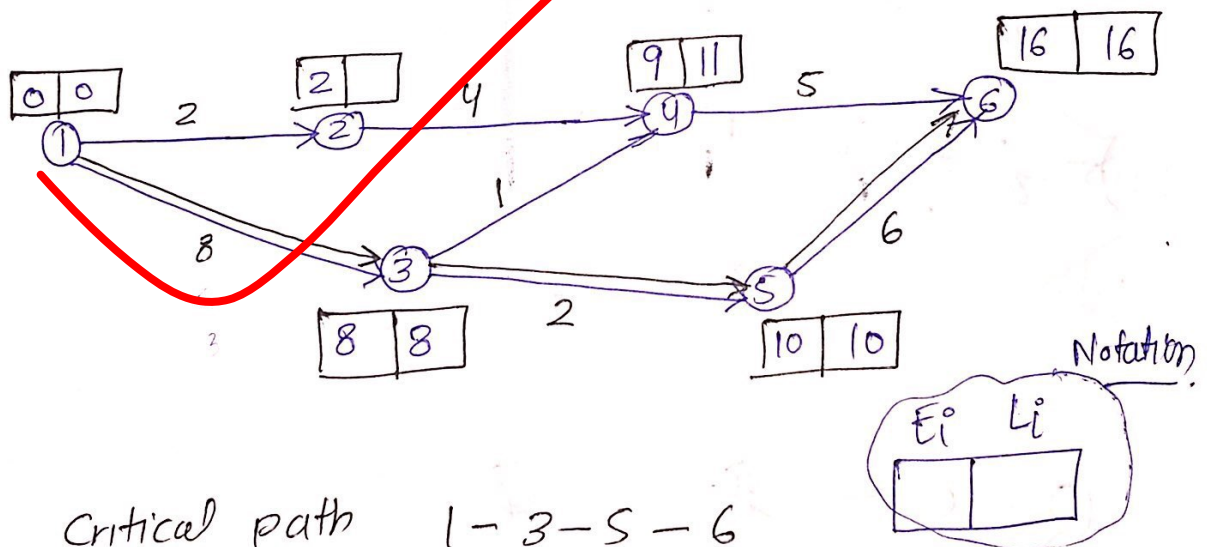
- Tracking mechanism is used



to focus sun rays.

6b

Activity (i-j)	Time Est (week)		Direct cost est (1000)		Cost slope ($\Delta C/\Delta t$)
	Normal	Crash	Normal	Crash	
1-2	2	1	10	15	5
1-3	8	5	15	21	2
2-4	4	3	20	24	4
3-4	1	1	7	7	—
3-5	2	1	8	15	7
4-6	5	3	10	16	3
5-6	6	2	12	36	6



Critical path 1-3-5-6

Normal completion time = 16 weeks

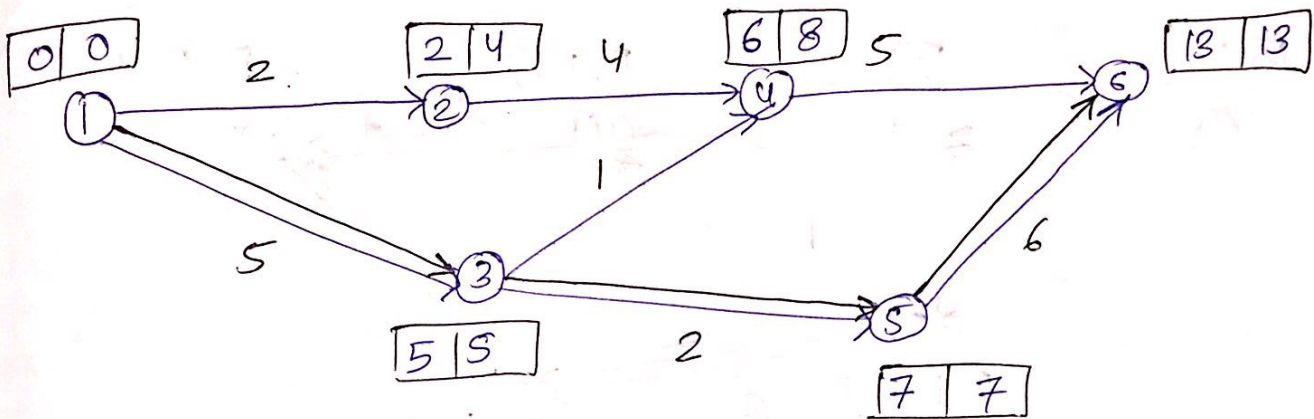
Total Normal cost = Direct cost + Indirect cost

Direct cost = 82 thousands

Ind. cost = $5 \times 16 = 80$ thousand

$T_c = 82 + 80 = 162$ thousand

Now crashing the activity 1-3 by 3 days



$$T_E = 13 \text{ day}$$

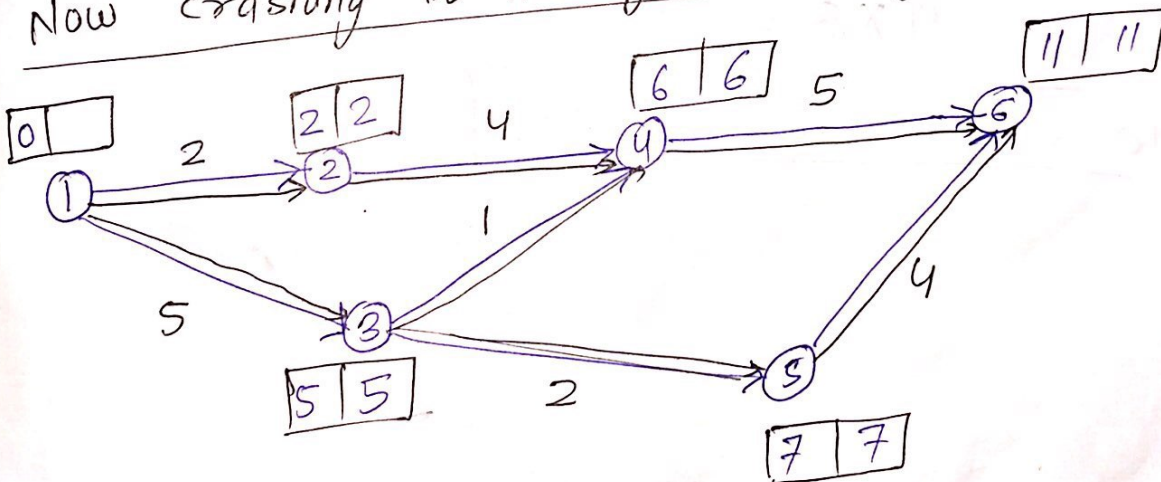
$$T_C = DC + IDC$$

$$DC = 82 + 3 \times 2 = 88 \text{ thousand}$$

$$IDC = 5 \times 13 = 65 \text{ thousand}$$

$$T_C = 153 \text{ thousand}$$

Now crashing the Activity 5-6 by 2 days.



all paths are critical path

1-2-4-6

1-3-4-6

1-3-5-6

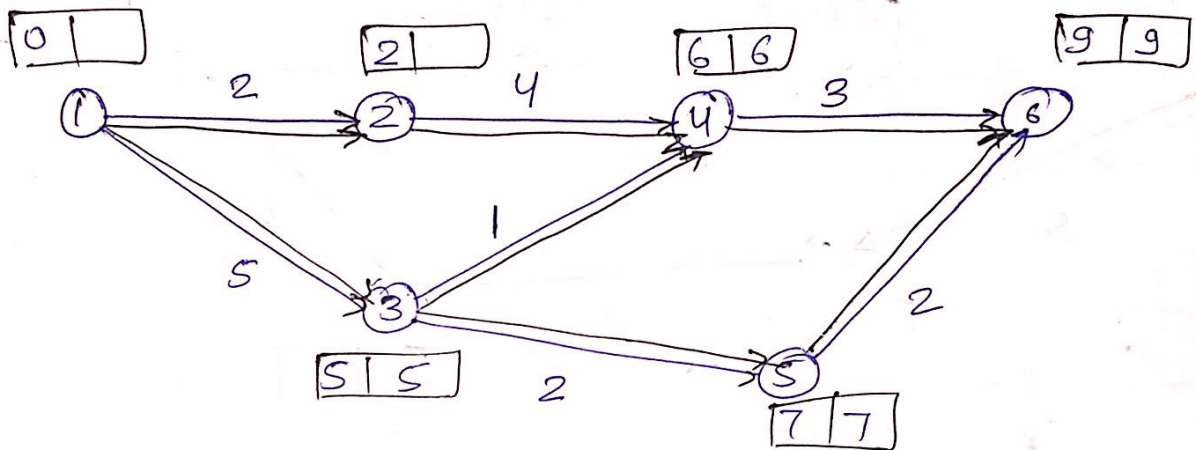
$$T_C = DC + IDC$$

$$DC = 82 + 3 \times 2 + 2 \times 6 = 100 \text{ th}$$

$$IDC = 5 \times 11 = 55$$

$$T_C = 155 \text{ thousand}$$

Now options (4-6) & 5-6 crashing by 2 days
~~(1-2)~~ & ~~(3-4)~~



all are critical path.

$$T_E = 9 \text{ days}$$

$$T_C = DC + IDC$$

$$DC = 8 \times 2 + 3 \times 2 + 6 \times 2 + 3 \times 2 + 6 \times 2$$

$$= ₹18 \text{ thousands Rs}$$

$$IDC = 9 \times 5 = 45$$

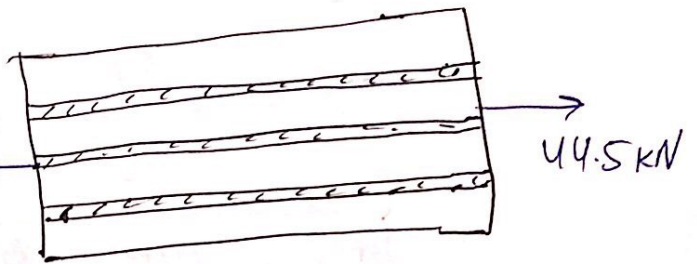
$$T_C = 163 \text{ thousand Rs.}$$

19

6③

70% poly.C — Matrix

30% Aramid — fibre



$$A = 320 \text{ mm}^2$$

deformation in both will be same.

$P_m \rightarrow$ Load on matrix

$A_m \rightarrow$ Area of "

$P_f \rightarrow$ Load on fibre

$A_f \rightarrow$ Area "

$$\Delta_f = \Delta_m$$

$$\frac{P_f \cdot L}{A_f \cdot E_f} = \frac{P_m \cdot L}{A_m \cdot E_m}$$

$$\frac{P_f}{P_m} = \frac{A_f \cdot E_f}{A_m \cdot E_m} = \frac{0.3 \times 131}{0.7 \times 2.4}$$

$$\frac{P_f}{P_m} = 23.393$$

$$P_f - 23.393 P_m = 0 \quad \text{--- (1)}$$

$$P_f + P_m = 44.5 \text{ kN} \quad \text{--- (2)}$$

Solving (1) & (2)

$$\begin{aligned} P_f &= 42.67 \text{ kN} \\ P_m &= 1.824 \text{ kN} \end{aligned}$$

stress on fibre

$$\sigma_f = \frac{P_f}{A_f} = \frac{42.67 \times 10^3}{820 \times 0.3}$$

$$\sigma_f = 444.48 \text{ MPa}$$

stress on Matrix

$$\sigma_m = \frac{P_m}{A_m} = \frac{1.824 \times 10^3}{0.7 \times 320} = 8.14 \text{ MPa}$$

strain in composite

$$E_m = E_f \quad \epsilon = \frac{\sigma}{E} = \frac{\sigma_f}{E_f} = \frac{\sigma_m}{E_m}$$

$$\epsilon = \frac{444.48}{131 \times 10^3} = 3.393 \times 10^{-3}$$

20

8@

1. Submerged Arc Welding :-

- Submerged arc welding is used to weld high thickness plates.

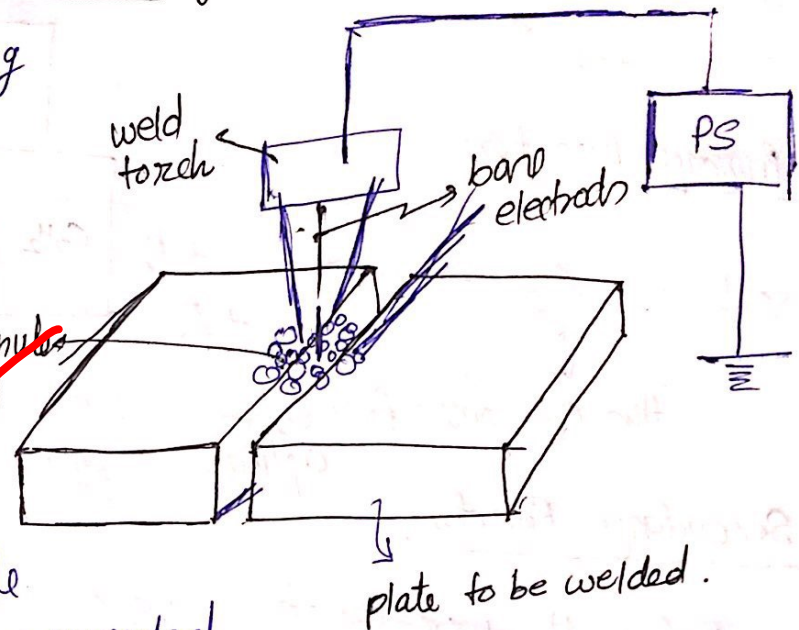
* Submerged Arc welding used in many products.

* the current flows through bare electrode.

& the arc is surrounded by the Granules of CaF_2 .

* these Granules avoid the UV rays to come out.

* Granules prevent weld spatter & prevent from oxide formation.

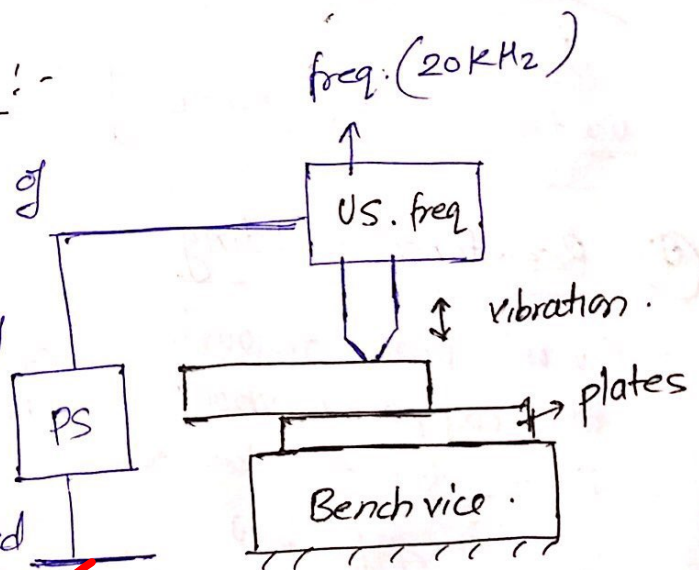


2. Ultrasonic Welding :-

- It comes to the category of the solid state welding.
- It utilizes the high frequency about 20 KHz.

Due to the rubbing action & friction heat is generated & hence pressure is applied to it.

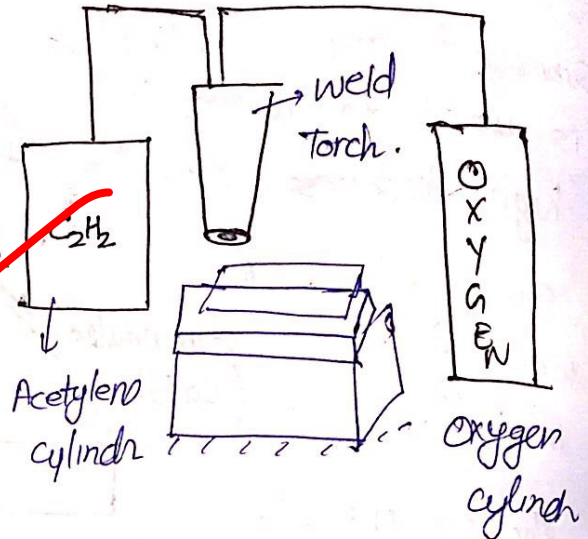
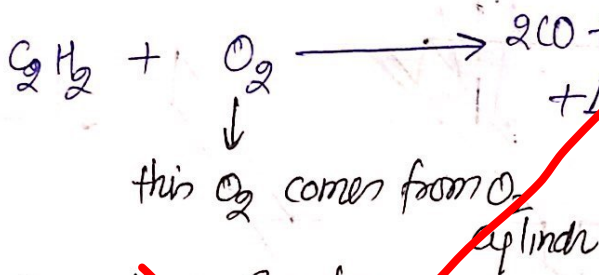
to weld by the other plate. less heat affected zone will be produced & there will not be any tendency to form oxide formation.



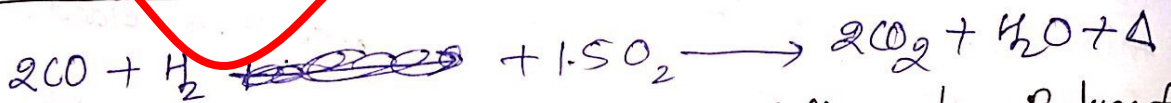
③ GAS Welding :-

Gas welding utilises chemical energy to joint 2 metals.

Primary Reaction.



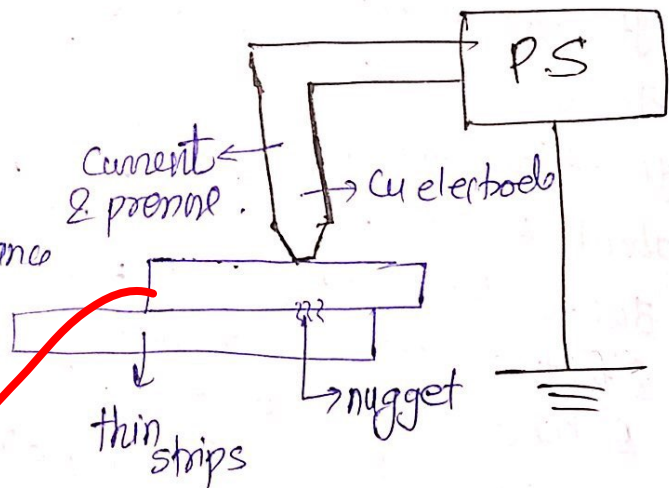
Secondary Reaction.



oxidising flame	Neutral flame	Reduction flame
$\frac{O_2}{C_2H_2} > 1$ 1600°C 3200°C use for Cu, Brass, Bronze	$\frac{O_2}{C_2H_2} = 1$ 1600°C 3100°C use for MS, stainless steel	$\frac{O_2}{C_2H_2} < 1$ 1600°C 2900°C use for CI, HCS

④ Resistance welding

- Current passes through the copper electrodes
- hence due to Resistance of air gap b/w plate, when current passes through it heat is generated

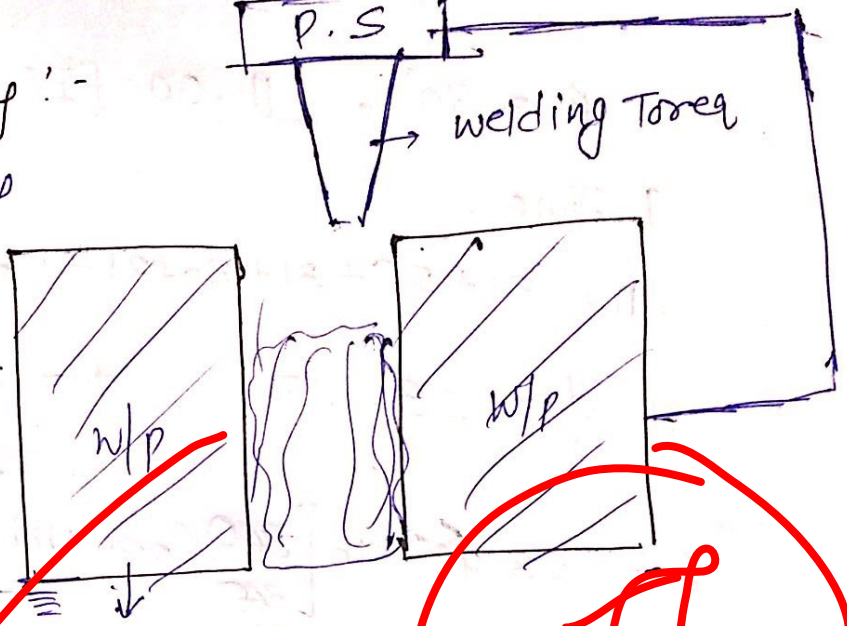


→ that heat utilized to melt & then pressure is applied that weld the thin strip.

→ ~~Acetylene~~ ~~oxygen~~ used for thin plates.

Electroslag Welding :-

- This welding Technique is used for the thick plates and high thickness of weld

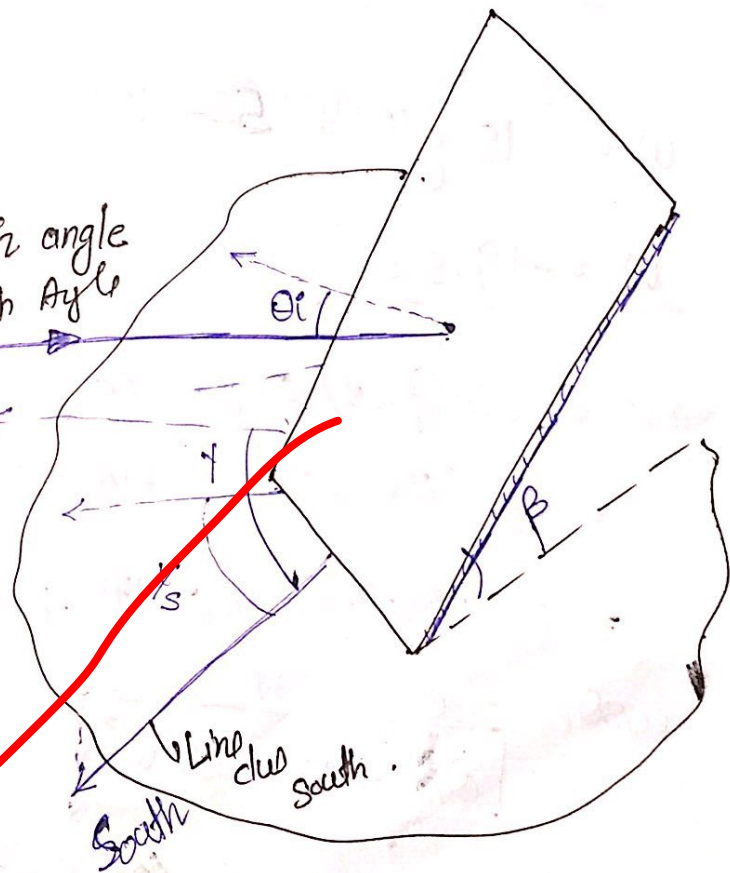


- Electroslag welding is done only in the horizontal

- because the thickness is high.
- the molten metal swims on the weld pool & metal is filled by weld torch

Q-8 (b)

- $\gamma \rightarrow$ Solar Azimuth angle
- $\gamma_s \rightarrow$ surface Azimuth Angle
- $\beta \rightarrow$ tilt angle
- $\theta_i \rightarrow$ Incidence angle
- $\delta \rightarrow$ declination



$$\beta = 30^\circ, \quad 11.00 \text{ [IST]}$$

1 June

$$n = 31 + 29 + 31 + 30 + 31 + 1 = 153$$

$$\phi = 28^\circ 35', \quad \phi = 28.583^\circ$$

$$\begin{aligned} \delta &= 23.45 \sin \left[\frac{360}{365} (284 + n) \right] \\ &= 23.45 \sin \left[\frac{360}{365} (284 + 153) \right] \\ &= \cancel{23.45} 22.174^\circ \end{aligned}$$

$$\begin{aligned} \text{LAT} &= 11:00 - 4 \left[\left(81 + \frac{44}{60} \right) - \left(77 + \frac{12}{60} \right) \right] \\ &= 10:41:52 \end{aligned}$$

$$w = 15 \left[10:41:52 - 12:00:00 \right]$$

$$w = -19.533^\circ$$

$$\begin{aligned} \cos \theta_i &= \sin(\phi - \beta) \sin \delta + \cos(\phi - \beta) \cos \delta \cos w \\ &= \sin(28.583 - 30) \sin(22.174) + \cos(28.583 - 30) \cos(22.174) \cos(-19.533) \\ &= \sin(28.583 - 30) \sin(22.174) + \cos(28.583 - 30) \cos(22.174) \cos(-19.533) \\ \cos \theta_i &= 0.86314 \end{aligned}$$

$$\theta_i = 30.328^\circ$$

$$\begin{aligned} \text{No of day hours} &= \frac{2}{15} \cos^{-1} (-\tan \phi \cdot \tan \delta) = \frac{2}{15} \cos^{-1} (-\tan 28.583^\circ \cdot \tan 22.174^\circ) \\ &= 13.71 \text{ hours} \end{aligned}$$

Q- 8 (C)

$$\alpha = 0.2$$

Month	Demand (unit)	Forecast (u)	Error
March	350	400	-50
April	440	390	50
May	450	400	50
June	460	410	50
July	495	420	75
Aug	510	435	75

Forecast for next month (April)

$$\begin{aligned}
 F_t &= F_{t-1} + \alpha (D_{t-1} - F_{t-1}) \\
 &= 400 + (0.2)(-50) \\
 &= 390
 \end{aligned}$$

Forecast of month May

$$\begin{aligned}
 F_t &= F_{t-1} + \alpha (D_{t-1} - F_{t-1}) \\
 &= 390 + (0.2)(50) \\
 &= 400
 \end{aligned}$$

Forecast for month June

$$\begin{aligned}
 F_t &= F_{t-1} + \alpha (D_{t-1} - F_{t-1}) \\
 &= 400 + 0.2(50) = 410
 \end{aligned}$$

Forecast for month July

$$\begin{aligned}
 F_t &= F_{t-1} + \alpha (D_{t-1} - F_{t-1}) \\
 &= 410 + 0.2(50) = 420
 \end{aligned}$$

Forecast of the month Aug

$$\begin{aligned} F_t &= F_{t-1} + \alpha (D_{t-1} - F_{t-1}) \\ &= 420 + 0.2(75) \\ &= 435 \end{aligned}$$

$$\text{Tracking signal} = \frac{\text{RSFE}}{\text{MAD}}$$

$$\begin{aligned} \text{Running sum forecast error} &= \$ \\ &= -50 + 50 + 50 + 50 + 75 + 75 \end{aligned}$$

$$\begin{aligned} \text{RSFE} &= 250 \\ \text{MAD} &= \frac{50 + 50 + 50 + 50 + 75 + 75}{6} = 58.333 \end{aligned}$$

$$\text{Tracking signal} = \frac{\text{RSFE}}{\text{MAD}} = \frac{250}{58.333}$$

$$= 4.2857$$