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ELECTRONIC DEVICES

ELECTRONICS ENGINEERING

Date of Test : 10/06/2024

ANSWER KEY >

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|--------|---------|---------|---------|---------|
| 1. (a) | 7. (c) | 13. (a) | 19. (b) | 25. (c) |
| 2. (c) | 8. (c) | 14. (a) | 20. (d) | 26. (b) |
| 3. (b) | 9. (a) | 15. (c) | 21. (a) | 27. (b) |
| 4. (c) | 10. (b) | 16. (b) | 22. (b) | 28. (a) |
| 5. (a) | 11. (b) | 17. (b) | 23. (c) | 29. (a) |
| 6. (a) | 12. (b) | 18. (b) | 24. (c) | 30. (c) |

DETAILED EXPLANATIONS

1. (a)
Zener breakdown voltage is less because in higher doping region, depletion layer width is small and a small reverse voltage is able to break the covalent bond and gives sudden increase in current.
Hence, zener breakdown voltage V_1 corresponds to point A.

2. (c)
We know that,
Collector current, $I_C = \beta I_B + (1 + \beta)I_{CO}$
 $I_C = \beta I_B + \beta I_{CO} + I_{CO}$
 $\therefore \beta = \frac{I_C - I_{CO}}{I_B + I_{CO}}$

but, $\alpha = \frac{\beta}{1 + \beta} = \frac{\frac{I_C - I_{CO}}{I_B + I_{CO}}}{1 + \frac{I_C - I_{CO}}{I_B + I_{CO}}} = \frac{I_C - I_{CO}}{I_B + I_{CO} + I_C - I_{CO}}$

 $\therefore \alpha = \frac{I_C - I_{CO}}{I_C + I_B}$

3. (b)
Given, Oxide thickness (t_{ox}) = 50 nm
Capacitance per unit area, $C = \frac{\epsilon_{ox}}{t_{ox}} = \frac{3.45 \times 10^{-11}}{50 \times 10^{-9}} \text{ F/m}^2 = 6.9 \times 10^{-4} \text{ F/m}^2$
 $\therefore C = 69 \text{ nF/cm}^2$

4. (c)
Given, Collector current, $I_C = 1 \text{ mA}$
Since, $I_C = 1 \text{ mA} > 0 \Rightarrow$ BJT not in cut-off region.
Emitter current $I_E = 1.2 \text{ mA}$
But $I_E = I_B + I_C$
 $\Rightarrow I_B = I_E - I_C = 0.2 \text{ mA}$
 $\beta = \frac{I_C}{I_B} = \frac{1 \text{ mA}}{0.2 \text{ mA}} = 5 < \beta_{\min}$
 \therefore BJT is in saturation region.

5. (a)
The conductors have the positive temperature coefficient of resistance. The conductors have almost linear increase in resistivity.

6. (a)
In a forward biased pn-junction diode, the current flow is due to diffusion of majority carriers and recombination of minority carriers.

7. (c)

$$\frac{D_n}{\mu_n} = \frac{D_p}{\mu_p} = V_T \quad (\text{Einstein's equation})$$

$$\Rightarrow \frac{48}{\mu_n} = \frac{12}{\mu_p}$$

$$\Rightarrow 4 = \frac{\mu_n}{\mu_p}$$

$$\mu_p + \mu_n = 100 \quad (\text{given})$$

$$5\mu_p = 100$$

$$\mu_p = 20$$

$$\mu_n = 80 \text{ cm}^2/\text{V-sec}$$

8. (c)

Given, resistivity, $\rho = 1.5 \text{ } \Omega\text{-cm}$

Hall coefficient, $R_H = -1250 \text{ cm}^3/\text{C}$

Since, R_H is negative, the charge carriers are electrons.

Mobility, $\mu_e \approx \sigma |R_H|$

$$= \frac{1}{\rho} |R_H| = \frac{1}{1.5} \times 1250$$

$$\therefore = 833 \text{ cm}^2/\text{V-sec}$$

9. (a)

$$\alpha = \beta^* \gamma$$

$$\gamma = \text{emitter injection efficiency, } \gamma = \frac{98}{100} = 0.98$$

$$\beta^* = \text{base transport factor, } \beta^* = \frac{99 - 1.98}{99} = 1 - \frac{2}{100} = 0.98$$

$$\alpha = \text{common base current gain} = \gamma\beta^* = 0.98 \times 0.98 = 0.9604$$

10. (b)

$$\lambda \leq \frac{1.24}{E_g \text{ (in eV)}} \mu\text{m}$$

$$\lambda_{(\text{max})} = \frac{1.24}{2.5} \mu\text{m} = 0.496 \mu\text{m} = 4960 \text{ \AA}$$

11. (b)

Given, MOSFET is operated in saturation region and channel length modulation is present,

$$\therefore \text{ Drain current, } I_D = \mu_n C_{ox} \frac{W}{2L} (V_{GS} - V_T)^2 [1 + \lambda V_{DS}] \quad \dots(i)$$

Drain to source conductance,

$$g_{ds} = \frac{\partial I_D}{\partial V_{DS}} = \mu_n C_{ox} \frac{W}{2L} (V_{GS} - V_T)^2 (\lambda) \quad \dots(ii)$$

From equation (i), we can write,

$$\frac{I_D}{1 + \lambda V_{DS}} = \mu_n C_{ox} \frac{W}{2L} (V_{GS} - V_T)^2$$

We can re-write equation (ii) as,

$$g_{ds} = \frac{I_D}{1 + \lambda V_{DS}} \cdot \lambda$$

or,

$$g_{ds} = \frac{I_D}{\frac{1}{\lambda} + V_{DS}}$$

12. (b)

The current,

$$I_D = \frac{5 \text{ V} - 1.6 \text{ V}}{R}$$

$$I_D = \frac{3.4 \text{ V}}{R} \quad \dots(i)$$

But it is given, to produce 1 mcd, $I_{D(\min)} = 4 \text{ mA}$

So,

$$\frac{3.4 \text{ V}}{R} \geq 4 \text{ mA}$$

$$R \leq \frac{3.4}{4} \text{ k}\Omega = 850 \Omega$$

$$R_{(\max)} = 850 \Omega$$

13. (a)

$$P_n = P_{n0} e^{0.5/V_i}$$

$$P_{n0} = \frac{n_i^2}{n_{n0}} = \frac{10^{20}}{5 \times 10^{15}} = 2 \times 10^4 \text{ cm}^{-3}$$

$$P_n = 2 \times 10^4 e^{20} \approx 10 \times 10^{12} \text{ cm}^{-3}$$

14. (a)

The Fermi potential,

$$\phi_{fp} = \frac{kT}{q} \ln \left[\frac{N_a}{n_i} \right]$$

$$\phi_{fp} = 0.026 \ln \left[\frac{10^{16}}{1.5 \times 10^{10}} \right]$$

$$\phi_{fp} = 0.35 \text{ V}$$

The maximum space charge width

$$x_{d(\max)} = \left[\frac{4\epsilon_{si}\phi_{fp}}{eN_a} \right]^{1/2} = \left[\frac{4 \times 1.04 \times 10^{-12} \times 0.35}{1.6 \times 10^{-19} \times 10^{16}} \right]^{1/2} \text{ cm}$$

$$= 3.02 \times 10^{-5} \text{ cm}$$

$$x_{d(\max)} = 0.302 \mu\text{m}$$

15. (c)

Given current equation of a PN junction diode is,

$$I(T) = I_s(T_0) \exp [0.057 (T - T_0)] ; T_0 = 300 \text{ K}$$

$$I(T) = I_s (300) \exp [0.057 (T - 300)] \quad \dots(i)$$

At $T = 300 \text{ K}$,

$$I(300) = I_s (300) \exp [0.057 (300 - 300)]$$

$$\therefore I(300) = I_s (300) \quad \dots(ii)$$

It is given that, at a temperature (assume T_1) the current is twice its value at $T = 300 \text{ K}$.

The new current at T_1 is

$$I(T_1) = 2I (300) \quad \dots(iii)$$

But,

$$I(T_1) = I_s (300) \exp [0.057 (T_1 - 300)] \quad \dots(iv)$$

Substitute equation (iii) in equation (iv),

$$2I (300) = I_s (300) \exp [0.057 (T_1 - 300)]$$

From equation (ii),

$$I (300) = I_s (300)$$

$$2I_s (300) = I_s (300) \exp [0.057 (T_1 - 300)]$$

$$2 = \exp [0.057 (T_1 - 300)]$$

$$\ln 2 = 0.057 (T_1 - 300)$$

$$\therefore T_1 = 312.16 \text{ K}$$

$$T_1 = 313 \text{ K}$$

16. (b)

Given that,

Reverse saturation current density, $J_s = 3.6 \times 10^{-11} \text{ A/cm}^2$

Photo current density, $J_L = 15 \text{ mA/cm}^2$

The open-circuit voltage of a solar cell is,

$$V_{OC} = V_t \ln \left[1 + \frac{J_L}{J_s} \right] = 0.026 \ln \left[1 + \frac{15 \times 10^{-3}}{3.6 \times 10^{-11}} \right]$$

$$V_{OC} = 0.516 \text{ V}$$

17. (b)

Diffusion potential (or) built in potential,

$$V_{bi} = \text{Area under the electric field distribution curve}$$

$$= \text{Area under given curve (which resembles triangle)}$$

$$V_{bi} = \frac{1}{2} \times \text{Base} \times \text{height} = \frac{1}{2} \times (W_p + W_N) \times (-E)$$

magnitude of diffusion potential

$$|V_{bi}| = \left| \frac{1}{2} \times (W_p + W_N) \times (-E) \right|$$

$$= \frac{1}{2} \times 4 \mu\text{m} \times 15 \times 10^4 \text{ V/m}$$

$$|V_{bi}| = 0.3 \text{ V}$$

18. (b)

As drain is connected to gate for both MOSFETs, they will be in saturation mode of operation.

i.e., $I_{D1} = I_{D2}$
 $K_1(V_{GS1} - V_T)^2 = K_2(V_{GS2} - V_T)^2$

Since, $K \propto W$; $K_2 = 2K_1$

$$K_1(V_{GS1} - V_T)^2 = 2K_1(V_{GS2} - V_T)^2$$

But $V_{GS1} = 5 - V_0$

$$V_{GS2} = V_0$$

$$(5 - V_0 - 1.5)^2 = 2(V_0 - 1.5)^2$$

$$3.5 - V_0 = \sqrt{2}(V_0 - 1.5)$$

$$3.5 - V_0 = \sqrt{2} V_0 - 2.12$$

$$2.414 V_0 = 5.62$$

$$V_0 = 2.33 \text{ V}$$

19. (b)

$$C_T \propto \frac{1}{\sqrt{V_{bi} + V_{RB}}}$$

$$\frac{C_{T1}}{C_{T2}} = \frac{\sqrt{V_{bi} + V_{RB2}}}{\sqrt{V_{bi} + V_{RB1}}}$$

at $V_{RB1} = 0 \text{ V}$, $C_{T1} = 1 \mu\text{F}$.

at $V_{RB2} = -6 \text{ V}$, $C_{T2} = 0.5 \mu\text{F}$.

$$\frac{C_{T1}}{C_{T2}} = \frac{\sqrt{V_{bi} + V_{RB2}}}{\sqrt{V_{bi} + V_{RB1}}}$$

$$\frac{1}{0.5} = \sqrt{\frac{-6 + V_{bi}}{V_{bi}}}$$

$\therefore V_{bi} = -2 \text{ V}$

20. (d)

We know that,

Diode voltage V_D decreases by 2.5 mV per 1°C rise in temperature.

Given, temperature, $T_1 = 20^\circ\text{C}$

$$\frac{\Delta V_D}{\Delta T} = -2.5 \text{ mV}/^\circ\text{C}$$

$$\frac{V_{D2} - V_{D1}}{(T_2 - 20)} = -2.5 \times 10^{-3}$$

$\therefore \frac{(600 - 700) \times 10^{-3}}{-2.5 \times 10^{-3}} = T_2 - 20$

$\therefore T_2 = 60^\circ\text{C}$

21. (a)

We know that,

$$\text{Potential function, } \phi_s = V_T \ln\left(\frac{n_0}{n_i}\right)$$

$$\text{or, } \phi_s = V_T \ln\left[\frac{N_D}{n_i}\right]$$

Let potential at 1 μm distance is ϕ_{s1} ,

$$\therefore \phi_{s1} = V_T \ln\left[\frac{N_{D2}}{n_i}\right] \quad \dots(\text{i})$$

$$\phi_{s1} = V_T \ln\left[\frac{10^{16}}{n_i}\right]$$

Let potential at 2 μm distance is ϕ_{s2} ,

$$\therefore \phi_{s2} = V_T \ln\left[\frac{N_{D1}}{n_i}\right] \quad \dots(\text{ii})$$

It is given magnitude of potential difference,

$$\text{i.e., } |\phi_{s1} - \phi_{s2}| = 0.12 \text{ V}$$

$$V_T \ln\left[\frac{N_{D2}}{N_{D1}}\right] = 0.12 \text{ V}$$

$$\therefore \frac{N_{D2}}{N_{D1}} = e^{\frac{0.12}{0.026}}$$

$$\Rightarrow N_{D1} = 9.89 \times 10^{13} \text{ cm}^{-3}$$

22. (b)

Since two MOSFETs are operated in saturation mode,

$$I_{DN} = \mu_n C_{ox} \frac{W_n}{2L} (V_{GSN} - V_{TN})^2$$

$$\text{or, } I_{DN} = \mu_n C_{ox} \frac{W_n}{2L} (V_{OV})^2$$

where, overdrive voltage $V_{OV} = V_{GSN} - V_{TN}$

$$\text{Similarly, } I_{DP} = \mu_p C_{ox} \frac{W_p}{2L} (V_{GSP} - V_{TP})^2$$

$$\text{or, } I_{DP} = \mu_p C_{ox} \frac{W_p}{2L} (V_{OV})^2$$

where, overdrive voltage $V_{OV} = V_{GSP} - V_{TP}$ given, $I_{DN} = I_{DP}$

$$\mu_n C_{ox} \frac{W_n}{2L} (V_{OV})^2 = \mu_p C_{ox} \frac{W_p}{2L} (V_{OV})^2$$

$$\therefore \frac{W_n}{W_p} = \frac{\mu_p}{\mu_n} = 0.4$$

In the given question, it is asking that,

$$\frac{W_p}{W_n} = \frac{1}{0.4} = 2.5$$

23. (c)

24. (c)

Fill factor of solar cell is,

$$\text{F.F.} = \frac{\text{Maximum power obtained}}{V_{oc} \times I_{sc}}$$

$$0.65 = \frac{65 \times 10^{-3}}{V_{oc} \times I_{sc}}$$

$$\therefore V_{oc} \times I_{sc} = \frac{65 \times 10^{-3}}{0.65} = 100 \text{ mW}$$

\(\therefore\) Option (c) satisfies the result (\(V_{oc} \times I_{sc} = 40 \text{ mA} \times 2.5 \text{ V} = 100 \text{ mW}\))

25. (c)

Given, $\mu_n C_{ox} \frac{W}{L} = 1.5 \times 10^{-3} \text{ A/V}^2$

$$V_T = 0.65 \text{ V}$$

$$V_{GS} = 4 \text{ V}$$

$$V_{DS} = 6 \text{ V}$$

Power dissipation in the MOSFET is,

$$P = V_{DS} \times I_{DS}$$

where, I_{DS} is drain to source saturation current.

Since the MOSFET is operating in saturation region,

$$I_{DS} = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_T)^2$$

$$= \frac{1}{2} \times 1.5 \times 10^{-3} (4 - 0.65)^2$$

$$I_{DS} = 8.42 \times 10^{-3} \text{ A}$$

Power dissipation, $P = 6 \times 8.42 \times 10^{-3}$

$$\therefore P = 50.50 \text{ mW}$$

26. (b)

The steady state increase in conductivity,

$$\Delta \sigma = q(\mu_n + \mu_p)(\delta p)$$

In steady state, $\delta p = g' \tau_{po}$

where, g' is the uniform generation rate.

$$\therefore \Delta \sigma = q(\mu_n + \mu_p)(g' \tau_{po})$$

$$2 = (1.6 \times 10^{-19}) (8500 + 400)g' \times 10^{-7}$$

$$\therefore g' = 1.404 \times 10^{22} \text{ cm}^{-3} \text{ s}^{-1}$$

27. (b)

$$J_p = -qD_p \frac{dp}{dx}$$

for

$$x \leq w,$$

$$\frac{dp}{dx} = \frac{p(0) - p_0}{0 - w} = \frac{-(p(0) - p_0)}{w}$$

$$J_p = \frac{qD_p (p(0) - p_0)}{w} = \text{positive constant}$$

for

$$x \geq w,$$

$$\frac{dp}{dx} = 0$$

⇒

$$J_p = 0$$

28. (a)

$$q \phi(x) = E_F - E_i(x)$$

$$q \phi(0) = E_F - E_i(0) = kT \ln \left(\frac{N_D(0)}{n_i} \right)$$

$$\phi(0) = \frac{kT}{q} \ln \left(\frac{N_D(0)}{n_i} \right)$$

$$\phi(x = 5\mu\text{m}) = \frac{kT}{q} \ln \left(\frac{N_D(5\mu\text{m})}{n_i} \right)$$

$$V_0 = \phi(0) - \phi(x = 5\mu\text{m}) = \frac{kT}{q} \ln \left(\frac{N_D(0)}{N_D(5\mu\text{m})} \right)$$

$$= 0.026 \ln \left(\frac{10^{20}}{10^{15}} \right) \text{ V} \simeq 0.3 \text{ V}$$

29. (a)

ϕ_s = surface potential

$$= \frac{1}{2} E_s W_{\text{dep}}$$

$$E_s = \frac{2\phi_s}{W_{\text{dep}}} = \frac{2 \times 0.035}{0.4} \text{ V}/\mu\text{m}$$

$$E_s = 0.175 \text{ V}/\mu\text{m}$$

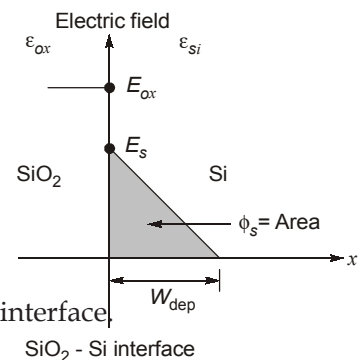
Boundary condition of electrostatic field should be satisfied at the interface

So,

$$\epsilon_{ox} E_{ox} = \epsilon_{si} E_s$$

$$E_{ox} = \frac{\epsilon_{si} E_s}{\epsilon_{ox}} = 3 E_s$$

$$E_{ox} = 0.525 \text{ V}/\mu\text{m}$$



$$E_{ox} = \frac{V_{ox}}{t_{ox}}$$

$$V_{ox} = E_{ox} t_{ox} = 0.525 \times 1.8 \text{ V} = 0.945 \text{ V}$$

$$V_G = V_{ox} + \phi_s = 0.98 \text{ V}$$

30. (c)

Force due to magnetic field, $\vec{F}_m = q\vec{v}_d \times \vec{B} = q\mu_p \vec{E}_{\text{applied}} \times \vec{B} = \frac{q\mu_p V_x}{L} \hat{x} \times (-10\hat{z})$

$$= \frac{100q\mu_p}{L} \hat{y}$$

\vec{F}_{ei} = force due to induced Hall electric field = $-\vec{F}_m$

$$= \frac{100q\mu_p}{L} (-\hat{y}) = q\vec{E}_{\text{ind}}$$

$$\vec{E}_{\text{ind}} = \frac{100\mu_p}{L} (-\hat{y})$$

As \vec{E}_{ind} in $(-\hat{y})$ direction, V_H is +ve

$$V_H = W|\vec{E}_{\text{ind}}| = \frac{W(100)\mu_p}{L} = \frac{W(100)(500 \times 10^{-4})}{2W} = 2.5 \text{ V}$$

