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CA	<b>STI</b> M	NG ECH	+W Iani	<b>/ELI</b> Cal	DIN	<b>G+</b>   GINE	F <b>O</b> Erii	RMI NG	NG
CA	STI M	NG ECF	<b>+W</b> IANI Date o	CAL of Test	EN( : 21/0	<b>G+</b> GINE 4/202	FO ERII 5	RMI NG	NG
	<b>STI</b> M Er Key	NG ECF	+W IANI Date o	CAL of Test	DIN EN( : 21/0	<b>G+</b> GINE 4/202	FO ERII 5	RMI NG	NG
CA ANSWE	<b>STI</b> M E <b>R KEY</b> (c)		+W IANI Date o	/ELI CAL of Test	DIN ENC : 21/0	( <b>G+</b> ) GINE 4/202	FO ERII 5	RMI NG 25.	<b>NG</b> (b)
<b>ANSWE</b> 1. 2.	<b>STI</b> (c) (d)	NG EC⊢ [ 7. 8.	+ W	<b>/ELI</b> CAL of Test 13. 14.	CIN ENC : 21/0	( <b>G+</b> ) GINE 4/202 19. 20.	FO ERII 5 (c) (c)	<b>RMI</b> NG 25. 26.	<b>NG</b> (b) (c)
<b>ANSWE</b> 1. 2. 3.	<b>STI</b> (c) (d) (a)	NG ECH 7. 8. 9.	+ W	<b>/ELI</b> CAL of Test 13. 14. 15.	DIN ENC : 21/0 (d) (b) (b)	G+ GINE 4/202 19. 20. 21.	FO ERII 5 (c) (c) (b)	<b>RMI</b> NG 25. 26. 27.	NG (b) (c) (c)
<b>ANSWE</b> 1. 2. 3. 4.	<b>STI</b> (c) (d) (a) (b)	NG ECH 7. 8. 9. 10.	+ W	<b>/ELI</b> CAL of Test 13. 14. 15. 16.	DIN ENC : 21/0 (d) (b) (b) (a)	G+ GINE 4/202 19. 20. 21. 22.	FO ERII 5 (c) (c) (b) (c)	RMI NG 25. 26. 27. 28.	NG (b) (c) (c) (b)
<b>ANSWE</b> 1. 2. 3. 4. 5.	<b>STI</b> (c) (d) (a) (b) (c)	NG ECH 7. 8. 9. 10. 11.	+ W  AN  Date o (b) (a) (b) (a) (a)	<b>/ELI</b> CAL of Test 13. 14. 15. 16. 17.	CIN ENC : 21/0 (d) (b) (a) (d)	G+ GINE 4/202 19. 20. 21. 22. 23.	FO ERII 5 (c) (c) (b) (c) (a)	RMI NG 25. 26. 27. 28. 29.	NG (b) (c) (c) (b) (d)

# **DETAILED EXPLANATIONS**

### 1. (c)

High corrosion resistance

### 5. (c)

Due to high chemical activity among all structural metals, except aluminium and magnesium, brazing can join almost all metals.

### 6. (a)

Given: Voltage = 20 V, Current = 155 A, Heat transfer efficiency = 0.85 Net heat supplied =  $0.85 \times 20 \times 155 = 2635$  W Travel speed, v = 5 mm/sec Area of joint, a = 10 mm<sup>2</sup> Volume of base metal melted =  $5 \times 10 = 50$  mm<sup>3</sup>/sec Heat required for melting =  $50 \times 10 = 500$  J/sec = 500 W Melting efficiency =  $\frac{\text{Heat required for melting}}{\text{Net heat supplied}} \times 100\%$  $= \frac{500}{2635} \times 100 = 18.975\%$ 

## 7. (b)

Given: Volume of casting =  $(10)^3 = 1000 \text{ cm}^3$ 

Surface area of casting =  $6 \times 10^2 = 600 \text{ cm}^3$ 

Time required to solidify,  $T_s = r \left(\frac{V}{A}\right)^2$ 

$$T_{s} = 1.44 \times 10^{5} \text{ sec/m}^{2} \times \left(\frac{1000}{600} \text{ cm}\right)^{2}$$
$$= 1.44 \times 10 \text{ sec/cm}^{2} \times 2.778 \text{ cm}^{2} = 40 \text{ sec}$$
$$T_{s} = 40 \text{ sec}$$

9. (a)

Drawing ratio = 
$$\frac{D_b}{D_p} = \frac{225}{100} = 2.25$$

11. (a)

Dimension of wooden pattern = 
$$29 \times \left(1 + \frac{21}{1000}\right) \left(1 + \frac{13}{1000}\right) = 29.991 \text{ mm}$$

As,

13. (d)

$$\frac{\text{Corner radius}}{\text{Shell diameter}} = \frac{r}{d} = \frac{1.8}{40}$$
$$\frac{d}{r} > 20$$
Blank diameter =  $\sqrt{d^2 + 4dh} = \sqrt{40^2 + 4 \times 40 \times 60} = 105.83 \text{ mm}$ 

### 14. (b)

Combination die is similar to compound die except that here non cutting operations such as bending and forming are also included as part of operation.

16. (a)

 $\Rightarrow$ 

Length of contact, 
$$L_p = R \sin \alpha = \sqrt{R\Delta h}$$
  
 $\Delta h = 2R(1 - \cos \alpha)$   
 $5 = 2 \times 150 (1 - \cos \alpha)$   
 $\frac{5}{300} = 1 - \cos \alpha$   
 $\alpha = 10.4753^{\circ}$   
 $L_p = 150 \times \sin 10.4753^{\circ} = 27.27 \text{ mm}$   
Roll separating force,  $F = \sigma_0 L_p \times b = 195 \times 27.27 \times 100$   
 $= 0.531 \text{ MN}$ 

Ans. 27.5 mm, 0.531 MN



17. (d)

Energy expanded = 
$$\left(\frac{1}{2} \times 0.5 \times 300 + 300 \times 1.5\right) \times \frac{1 \text{MN}}{\text{m}^2} \times \text{m}^3$$
  
=  $(75 + 450) \times 1000 \text{ kJ} = 525000 \text{ kJ}$ 

18. (a)

Extrusion load, 
$$P = A_0 \sigma_0 \ln \frac{A_0}{A_f} = \frac{\pi}{4} \times 50^2 \times 365 \times \ln \left( \frac{\frac{\pi}{4} \times 50^2}{\frac{\pi}{4} \times 42.5^2} \right)$$
$$= \frac{\pi}{4} \times 50^2 \times 365 \times 2 \ln \left( \frac{50}{42.5} \right)$$
$$= 232946.7755 \text{ N} = 232.947 \text{ kN}$$

19. (c)

$$GF = \frac{mv^{2} / R}{mg} = \frac{v^{2}}{Rg}, \ v = \frac{\pi DN}{60}$$
$$= \frac{\pi^{2}D^{2}N^{2}}{3600 \times Rg} = \frac{\pi^{2} \times D^{2} \times N^{2} \times 2}{3600 \times D \times g} = \frac{\pi^{2} \times D^{2} \times N^{2}}{1800 \times g}$$
$$N = \sqrt{\frac{GF \times 1800 \times g}{\pi^{2}D}} = \frac{30}{\pi}\sqrt{\frac{2g(GF)}{D}}$$

here D is inner diameter of mold for horizontal centrifugal casting,

$$N = \frac{30}{\pi} \sqrt{\frac{2 \times 9.81 \times 60}{0.5073}} = 460 \, \text{rpm}$$

## 20. (c)

All three sum up to give resistance in resistance welding.

### 21. (b)

Large reduction or rolling using large diameter rolls leads to tensile stress on skin and compressive stress in bulk of metal.

### 22. (c)

Volume of casting = 
$$\frac{\pi}{4} \times (40)^2 \times 5 \text{ cm}^3$$
  
= 6283.185 cm<sup>3</sup>  
Extra volume needed = 15% of 6283.185  
Total volume of metal required = 7225.663 cm<sup>3</sup>

23. (a)

For

hot rolling  

$$(\Delta h)_{max} = \mu^2 R$$
  
 $(\Delta h)_{max} = (0.5)^2 \times 225 = 56.25 \text{ mm}$   
For cold rolling,  $(\Delta h)_{max} = (0.09)^2 \times 300 = 2.43 \text{ mm}$   
Factor  $= \frac{56.25}{2.43} = 23.148$ 

24. (b)

Sand density =  $1.6 \text{ g/cm}^3 = 0.0016 \text{ kg/cm}^3$ 

Volume of core = 
$$\frac{20}{0.0016}$$
 = 12500 cm<sup>3</sup>  
Density of Al-Cu alloy = 2.81 g/cm<sup>3</sup> = 0.00281 kg/cm<sup>3</sup>

9

Upward force = Weight of displaced Al-Cu alloy =  $12500 \times 0.00281 = 35.125$  kg Net upward force = Upward force - Weight of core =  $(35.125 - 20) \times 9.81 = 148.37$  N  $\approx 148.5$  N

#### 25. (b)

Melting factor in welding is defined as the proportional of the heat received at the work surface that is used for melting.

26. (c)

Electro gas welding, Electron beam welding, Laser beam welding are classified as fusion welding.

27. (c)

Increases flow stress: As strain rates increases, flow stress increases.

### 28. (b)

Mean flow stress 
$$(\overline{\sigma}_0) = \frac{k \in^n}{1+n}$$
  
 $k = 600 \text{ MPa}$   
 $n = 0.15$   
 $200 = \frac{600 \times \in^{0.15}}{1+0.15}$   
 $\epsilon = 1.67 \times 10^{-3}$   
 $\sigma = 600 (1.67 \times 10^{-3})^{0.15}$   
True stress,  $\sigma = 230 \text{ MPa}$ 

29. (d)

Spring back in a sheet metal bending operation is due to elastic recovery of metal.

30. (c)

Power supplied =  $0.7 \times 0.65 \times 22 \times 135 = 1351.35$  J Powered required =  $10.3 \times 5 \times AW$ (where, AW = Area of weld in mm<sup>2</sup>)  $1351.35 = 10.3 \times 5 \times AW$ Area of weld =  $26.24 \text{ mm}^2$ Volume of weld =  $26.24 \times 5 = 131.2 \text{ mm}^3/\text{sec}$ 

Area of filler wire = 
$$\frac{\pi}{4} \times (3.5)^2 = 9.62 \text{ mm}^2$$

Feed of filler wire (60% volume of filler) =  $\frac{0.6 \times 131.2}{9.62}$  = 8.18 mm/ sec

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