

GATE

Electrical Engineering

(Previous Years Solved Papers 1991-1995)

Contents

1. Electric Circuits	1 - 10
2. Signals and Systems	11 - 15
3. Electrical Machines	16 - 24
4. Power Systems	25 - 33
5. Control Systems	34 - 44
6. Electrical & Electronic Measurements	45 - 51
7. Analog Electronics	52 - 58
8. Digital Electronics	59 - 62
9. Power Electronics	63 - 68
10. Electromagnetic Theory	69 - 71
11. Engineering Mathematics	72 - 75



Electric Circuits

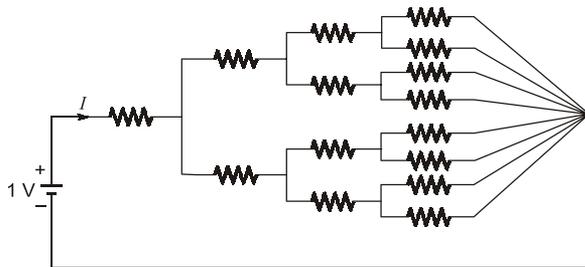
UNIT

I

CONTENTS

1. Basics 2
2. Steady State AC Analysis 3
3. Resonance and Locus Diagrams 4
4. Network Theorems 5
5. Transients and Steady State Response 6
6. Two Port Network and Network Functions 7
7. Magnetically Coupled Circuits,
Network Topology/Graph Theory & Filters 8
8. Three-Phase Circuits 9

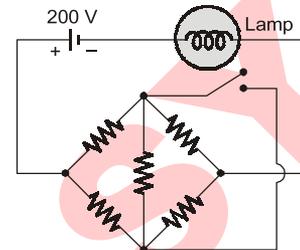
1.1 All resistances in the figure are $1\ \Omega$ each. The value of current ' I ' is



- (a) $\frac{1}{15}\text{ A}$
- (b) $\frac{2}{15}\text{ A}$
- (c) $\frac{4}{15}\text{ A}$
- (d) $\frac{8}{15}\text{ A}$

[1992 : 1 Mark]

1.2 All resistances in the circuit in figure are of R ohms each. The switch is initially open. What happens to the lamp's intensity when the switch is closed?



- (a) Increases
- (b) Decreases
- (c) Remains same
- (d) Answer depends on the value of R

[1992 : 1 Mark]

Answers Basics

1.1 (d) 1.2 (c)

Explanations Basics

1.1 (d)

$$\begin{aligned}
 R &= 1 + [(1 \parallel 1 + 1) \parallel (1 \parallel 1 + 1) + 1] \\
 &\quad \parallel [(1 \parallel 1 + 1) \parallel (1 \parallel 1 + 1) + 1] \\
 &= \frac{15}{8}\ \Omega \Rightarrow I = \frac{V}{R} = \frac{1}{15/8} = \frac{8}{15}\ \text{A}
 \end{aligned}$$

1.2 (c)

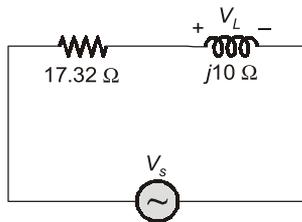
As the given bridge is balanced Wheatstone bridge, current flowing through the lamp will remain same irrespective of the state of switch; Hence intensity of lamp will remain same.



2

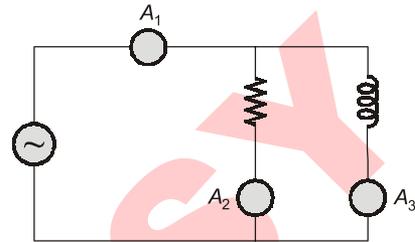
Steady State AC Analysis

2.1 In the circuit shown in figure, the voltage V_L has a phase angle of _____ with respect to V_s .



[1994 : 2 Marks]

2.2 In the circuit shown in figure, ammeter A_2 reads 12 A and A_3 reads 9 A. A_1 will read _____ A.



[1995 : 1 M]

Answers Steady State AC Analysis

2.1 (60) 2.2 (15)

Explanations Steady State AC Analysis

2.1 Sol.

$$V_L = V_s \times \frac{j10}{17.32 + j10}$$

(Using voltage division rule)

$$= V_s \times 0.5 \angle 60^\circ \text{ volts}$$

Hence, V_L has a phase angle of 60° with respect to V_s .

2.2 Sol.

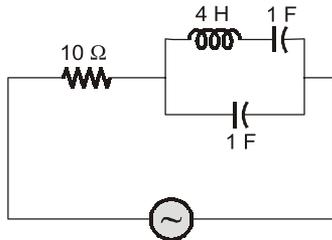
\therefore Current in resistor and inductor will be in quadrature for same voltage across them.

$$\therefore I_{A_1} = \sqrt{I_{A_2}^2 + I_{A_3}^2} = \sqrt{12^2 + 9^2}$$

$$= 15 \text{ A}$$

■■■■

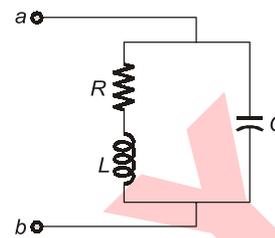
3.1 The following circuit shown in the figure resonates at



- (a) all frequencies (b) 0.5 rad/sec
(c) 5 rad/sec (d) 1 rad/sec

[1993 : 1 Mark]

3.2 At resonance, the given parallel circuit constituted by an iron-cored coil and a capacitor behaves like



- (a) an open-circuit
(b) a short-circuit
(c) a pure resistor of value R
(d) a pure resistor of value much higher than R

[1994 : 1 Mark]

3.3 A series R-L-C circuit has the following parameter values: $R = 10 \Omega$, $L = 0.01 \text{ H}$, $C = 100 \text{ mF}$. The Q-factor of the circuit at resonance is ____.

[1995 : 1 M]

Answers Resonance and Locus Diagrams

3.1 (b) 3.2 (d) 3.3 (0.032)

Explanations Resonance and Locus Diagrams

3.1 (b)

$$Z = 10 + \left(j4\omega - \frac{j}{\omega} \right) \parallel \left(-\frac{j}{\omega} \right)$$

$$= 10 - j \left[\frac{4 - \frac{1}{\omega^2}}{4\omega - \frac{2}{\omega}} \right]$$

For circuit to be in resonance imaginary part of Z must be equal to zero.

$$\text{Hence, } 4 - \frac{1}{\omega_{res}^2} = 0$$

$$\Rightarrow \omega_{res} = 0.5 \text{ rad/sec.}$$

3.2 (d)

$$Y = \frac{1}{R + j\omega L} \times \frac{R - j\omega L}{R - j\omega L} + \frac{1}{-jX_C}$$

$$Y = \frac{R - j\omega L}{R^2 + (\omega L)^2} + \frac{j}{X_C}$$

Imaginary parts are equal to zero for resonance

$$\frac{\omega L}{R^2 + (\omega L)^2} = \omega C$$

From this we get ' ω_0 '

At resonance,

$$Y = \frac{R}{R^2 + \omega_0^2 L^2} = \frac{1}{Y} = \frac{R^2 + \omega_0^2 L^2}{R}$$

$$Z \gg R$$

3.3 Sol.

$$Q_0 = 0.032$$

For series RLC circuit,

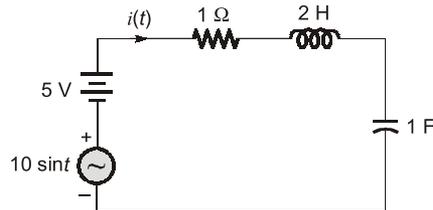
$$\text{Q-factor at resonance} = \frac{\omega_0 L}{R}$$

$$\omega_0 = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{(0.01) \times (100 \times 10^{-3})}}$$

$$= 10\sqrt{10} \text{ rad/sec.}$$

$$Q = \omega_0 \frac{L}{R} = \frac{10\sqrt{10} \times 0.01}{10} = 0.032$$

4.1 In the following circuit, $i(t)$ under steady state is



- (a) zero (b) 5
(c) $7.07 \sin t$ (d) $7.07 \sin(t - 45^\circ)$

[1993 : 1 Mark]

4.2 Superposition principle is not applicable to a network containing time-varying resistors. (True/False).

[1994 : 1 Mark]

■■■■

Answers Network Theorems

4.1 (d) 4.2 (F)

Explanations Network Theorems

4.1 (d)

For DC supply of 5 V, the capacitor acts as open circuit at the steady state, consequently there will not be any current flowing in the circuit due to DC supply.

For AC supply of $V = 10 \sin(t)$; $\omega = 1$ rad/sec.

$$\begin{aligned} Z &= R + j\omega L - \frac{j}{\omega C} = 1 + j2 - j \\ &= (1 + j) = \sqrt{2} \angle 45^\circ \Omega \end{aligned}$$

Hence, Current, $I = \frac{V}{Z}$

$$= \frac{10 \sin(t)}{\sqrt{2} \angle 45^\circ} = 7.07 \sin(t - 45^\circ) \text{ A}$$

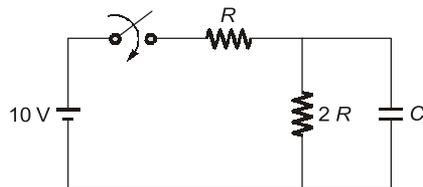
4.2 Sol.

False. Superposition principle is applicable on both time variant and time invariant resistors.

■■■■

Transients and Steady State Response

5.1 The time constant of the network shown in the figure is



- (a) $2RC$ (b) $3RC$
 (c) $\frac{RC}{2}$ (d) $\frac{2RC}{3}$

[1992 : 1 Mark]

Answers Transients and Steady State Response

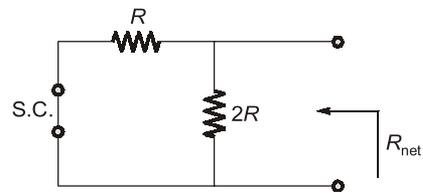
5.1 (d)

Explanations Transients and Steady State Response

5.1 (d)

Time constant, $\tau = R_{\text{net}} \cdot C$

R_{net} = Net resistance across capacitor when all the independent voltage sources are short circuited and all independent current sources are open circuited.



$$R_{\text{net}} = R \parallel 2R = \frac{2}{3}R$$

Hence time constant,

$$\tau = \frac{2}{3}RC \text{ sec.}$$



6

Two Port Network and Network Functions

6.1 If a two-port network is reciprocal, then we have, with the usual notation, the following relationship

- (a) $h_{12} = h_{21}$
- (b) $h_{12} = -h_{21}$
- (c) $h_{11} = h_{22}$
- (d) $h_{11} h_{22} - h_{12} h_{21} = 1$

[1994 : 1 Mark]

Answers Two Port Network and Network

6.1 (b)

Explanations Two Port Network and Network

6.1 (b)

For reciprocity,

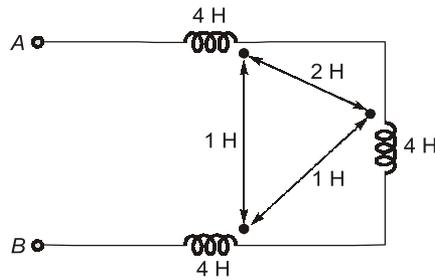
$$h_{12} = -h_{21}$$

For symmetry, $\begin{vmatrix} h_{11} & h_{12} \\ h_{21} & h_{22} \end{vmatrix} = 1$

■ ■ ■ ■

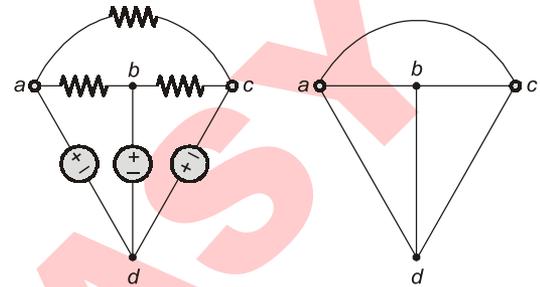
Magnetically Coupled Circuits, Network Topology/Graph Theory & Filters

7.1 The equivalent inductance seen at terminals A–B in the figure is H.



[1992 : 2 Marks]

7.2 The figure shows a DC resistive network and its graph is drawn a side. A 'proper tree' chosen for analysing the network will not contain the edges:



- (a) ab, bc, ad
- (b) ab, bc, ca
- (c) ab, bd, cd
- (d) ac, bd, ad

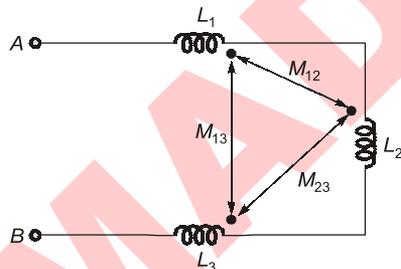
[1994 : 1 Mark]

Answers Magnetically Coupled Circuits, Network Topology/Graph Theory & Filters

7.1 (8) 7.2 (b)

Explanations Magnetically Coupled Circuits, Network Topology/Graph Theory & Filters

7.1 Sol.



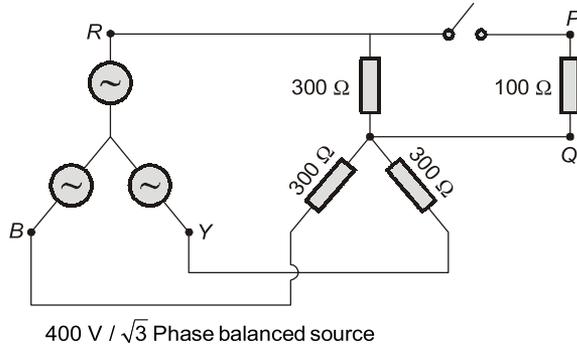
$$\begin{aligned}
 L &= L_1 + L_2 + L_3 - 2 M_{12} + 2 M_{23} - 2 M_{13} \\
 &= 4 + 4 + 4 - (2 \times 2) + (2 \times 1) - (2 \times 1) \\
 &= 8 \text{ H}
 \end{aligned}$$

7.2 (b)

Tree must not contain any closed loop. Hence, option (b) is correct.

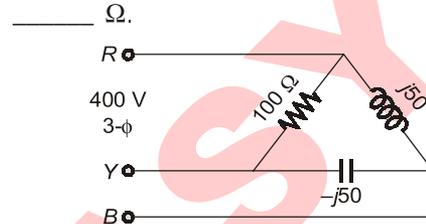


8.1 Using Thevenin equivalent circuit, determine the RMS value of the voltage across the 100 ohm resistor after the switch is closed in the 3-phase circuit shown in the figure.



[1992 : 2 Marks]

8.2 A set of 3 equal resistors, each of value R_x , connected in star across RYB of given figure consumes the same power as the unbalanced delta connected load shown. The value of R_x is



[1994 : 2 Marks]

Answers Three-Phase Circuits

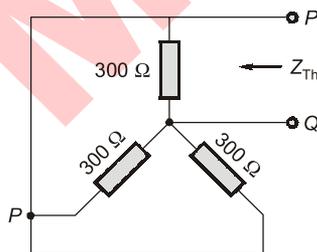
8.1 (115.5) 8.2 (100)

Explanations Three-Phase Circuits

8.1 Sol.

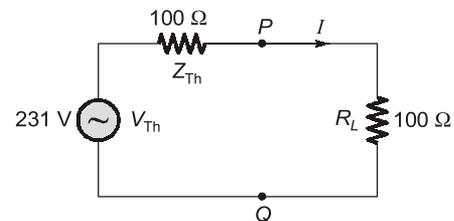
$$V_{Th} = V_{ph} = \frac{400}{\sqrt{3}} \approx 231V$$

Now, to find Z_{Th} , replacing all the independent voltage sources by short circuit, We have,



$$\therefore Z_{Th} = 300 \parallel 300 \parallel 300 = 100 \Omega$$

\therefore Thevenin's equivalent circuit:



\therefore Voltage across 100 Ω resistor

$$= 231 \times \frac{100}{100 + 100} \quad (\text{voltage division rule})$$

$$= \frac{231}{2} = 115.5 V$$

8.2 Sol.

∴ Only resistor consumes power, neither inductor nor capacitor.

∴ Power consumed in unbalanced delta

$$\text{connected load} = \frac{V_{ph}^2}{R} = \frac{V_L^2}{R} = \frac{(400)^2}{100} = 1600 \text{ W}$$

Power consumed in a balanced star connection containing a set of equal resistors (in all three phases), each of value

$$R_x = 3 \left[\frac{V_{ph}^2}{R_x} \right] = \frac{V_L^2}{R_x} = \frac{(400)^2}{R}$$

∴ According to the question, power consumed in both the cases is equal.

$$\therefore 1600 = \frac{(400)^2}{R} \Rightarrow R = 100 \Omega$$

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MADE EASY

Signals and Systems

UNIT

II

CONTENTS

1. Introduction of C.T. and D.T. Signals 12
2. Linear Time Invariant Systems 13
3. Laplace Transform 15

MADE

Introduction of C.T. and D.T. Signals

1.1 The value of the integral $\int_{-5}^{+6} e^{-2t} \delta(t-1) dt$ is equal to _____.

[1994 : 1 Mark]

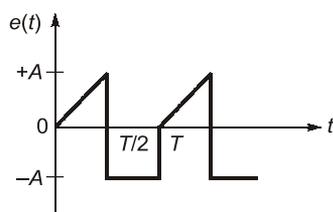
(a) $\sqrt{\frac{3}{2}} A$

(b) $\sqrt{\frac{2}{3}} A$

(c) $\sqrt{\frac{1}{3}} A$

(d) $\sqrt{2} A$ [1995 : 1 M]

1.2 The rms value of the periodic waveform $e(t)$, shown in the figure is



Answers Introduction of C.T. and D.T. Signals

1.1 (Sol.) 1.2 (b)

Explanations Introduction of C.T. and D.T. Signals

1.1 Sol.

Using, $\int_{-\infty}^{\infty} x(t) \delta(t-t_0) dt = x(t_0)$

We have, $\int_{-5}^{6} e^{-2t} \delta(t-1) dt = e^{-2}$

1.2 (b)

$$\begin{aligned} \text{RMS value} &= \left[\frac{1}{T} \left\{ \int_0^{T/2} \left(\frac{2A}{T} t \right)^2 dt + \int_{T/2}^T A^2 dt \right\} \right]^{1/2} \\ &= \sqrt{\frac{2}{3}} A \end{aligned}$$



2.1 $s(t)$ is step response and $h(t)$ is impulse response of a system. Its response $y(t)$ for any input $u(t)$ is given by

(a) $\frac{d}{dt} \int_0^t s(t-\tau) u(\tau) d\tau$

(b) $\int_0^t s(t-\tau) u(\tau) d\tau$

(c) $\iint_{00}^t s(t-\tau) u(\tau_1) d\tau_1 d\tau$

(d) $\frac{d}{dt} \int_0^t h(t-\tau) u(\tau) d\tau$

[1993 : 1 Mark]

2.2 If $f(t)$ is the step-response of a linear time-invariant system, then its impulse response is given by _____.

[1994 : 1 Mark]

2.3 The convolution of the functions $f_1(t) = e^{-2t} u(t)$ and $f_2(t) = e^t u(t)$ is equal to _____. [1995 : 1 M]

2.4 The impulse response of an initially relaxed linear system is $e^{-2t} u(t)$. To produce a response of $t e^{-2t} u(t)$, the input must be equal to

(a) $2 e^{-t} u(t)$

(b) $\frac{1}{2} e^{-2t} u(t)$

(c) $e^{-2t} u(t)$

(d) $e^{-t} u(t)$ [1995 : 1 M]

Answers Linear Time Invariant Systems

2.1 (a) 2.2 (Sol.) 2.3 (Sol.) 2.4 (c)

Explanations Linear Time Invariant Systems

2.1 (a)

$y(t) = u(t) * h(t)$ (always)
where $h(t)$ is impulse response
 $\therefore s(t)$ is step response (given)

$$\Rightarrow \frac{d}{dt} s(t) = h(t)$$

$$\therefore y(t) = u(t) * \frac{d}{dt} s(t)$$

$$= \frac{d}{dt} [u(t) * s(t)] \quad (\text{using property})$$

$$= \frac{d}{dt} \int_{-\infty}^{\infty} u(\tau) s(t-\tau) d\tau$$

(by definition of convolution)

$$= \frac{d}{dt} \int_0^t u(\tau) s(t-\tau) d\tau$$

($\because u(t)$ and $s(t)$ are causal functions)

2.2 Sol.

$$h(t) = \frac{d}{dt} f(t)$$

2.3 Sol.

$$\therefore f_1(t) = e^{-2t} u(t) \Rightarrow F_1(s) = \frac{1}{s+2}$$

$$\text{and } f_2(t) = e^t u(t) \Rightarrow F_2(s) = \frac{1}{s-1}$$

$$F_1(s) F_2(s) = \frac{1}{(s+2)(s-1)} = \frac{-1/3}{s+2} + \frac{1/3}{s-1}$$

$$\therefore F_1(s) \cdot F_2(s) = f_1(t) * f_2(t)$$

Multiplication in s-domain results in convolution in time domain.

$$\therefore f_1(t) * f_2(t) = \mathcal{L}^{-1} \left[\frac{-1/3}{s+2} + \frac{1/3}{s-1} \right]$$

$$= \left[-\frac{1}{3} e^{-2t} + \frac{1}{3} e^t \right] u(t)$$

2.4 (c)

$$H(s) = \mathcal{L}[e^{-2t}u(t)] = \frac{1}{s+2}$$

$$Y(s) = \mathcal{L}[te^{-2t}u(t)] = \frac{1}{(s+2)^2}$$

$$\Rightarrow X(s) = \frac{Y(s)}{H(s)} = \frac{1}{s+2}$$

Hence, input $x(t) = \mathcal{L}^{-1}[X(s)] = e^{-2t}u(t)$

■■■■

MADE EASY

3.1 The Laplace transformation of $f(t)$ is $F(s)$.

Given: $F(s) = \frac{\omega}{s^2 + \omega^2}$, the final value of $f(t)$ is

- (a) infinity (b) zero
(c) one (d) None of these

[1995 : 1 M]

Answers **Linear Time Invariant Systems**

3.1 (d)

Explanations **Linear Time Invariant Systems**

3.1 (d)

$$\therefore F(s) = \frac{\omega}{s^2 + \omega^2}$$

$\Rightarrow f(t) = \sin(\omega t) u(t)$ which is a periodic signal so final value theorem is not applicable on it.

Final value of $f(t)$ may be any value between -1 and $+1$.

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CONTENTS

1. D.C. Machines 17
2. Transformers 19
3. Three Phase Induction Machines 21
4. Synchronous Machines 22
5. Single Phase Induction Motors, Special Purpose Machines and Electromechanical Energy Conversion Systems 24

1.1 A separately excited DC motor has an armature resistance of 0.5 ohms. It runs from a 250 V DC supply drawing an armature current of 20 A at 1500 rpm. For the same field current, the torque developed for an armature current of 10 A will be _____.

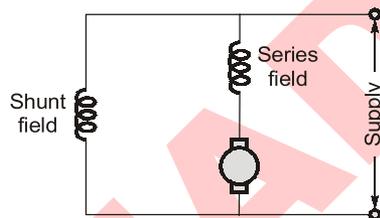
[1992 : 1 Mark]

1.2 Neglecting all losses, the developed torque (T) of a DC separately excited motor, operating under constant terminal voltage, is related to its output power (P) as under

- (a) $T \propto \sqrt{P}$ (b) $T \propto P$
 (c) $T^2 \propto P^3$ (d) T independent of P

[1992 : 1 Mark]

1.3 A cumulative compound long shunt motor is driving a load at rated torque and rated speed. If the series field is shunted by a resistance equal to the resistance of the series field, keeping the torque constant



- (a) the armature current increases
 (b) the motor speed increases
 (c) the armature current decreases
 (d) the motor speed decreases

[1993 : 1 Mark]

1.4 A differentially compounded DC motor with interpoles and with brushes on the neutral axis is to be driven as a generator in the direction with the same polarity of the terminal voltage. It will then

- (a) be a cumulatively compounded generator but the interpole coil connections are to be reversed.
 (b) be a cumulatively compounded generator without reversing the interpole coil connections.
 (c) be a differentially compounded generator without reversing the interpole coil connections.
 (d) be a differentially compounded generator but the interpole coil connections are to be reversed.

[1995 : 1 M]

1.5 A 4-pole dynamo with wave wound armature has 51 slots containing 20 conductors in each slot. The induced emf is 357 volts and the speed is 8500 rpm. The flux per pole will be

- (a) 3.5 mWb (b) 1.2 mWb
 (c) 14 mWb (d) 21 mWb [1995 : 2 M]

Answers D.C. Machines

1.1 (15.2788) 1.2 (b) 1.3 (a) 1.4 (b) 1.5 (b)

Explanations D.C. Machines

1.1 Sol.

$$\begin{aligned}
 V &= E_b + I_a R_a \\
 250 &= E_b + 20 \times 0.5 \\
 E_b &= 240 \text{ V} \\
 T &= \frac{P}{\omega} = \frac{E_b I_a}{2\pi N} = \frac{240 \times 10 \times 60}{2\pi \times 1500} \\
 &= 15.2788 \text{ Nm}
 \end{aligned}$$

1.2 (b)

$$\begin{aligned}
 T &= K\phi I_a \\
 T &\propto I_a \quad \dots(i)
 \end{aligned}$$

$$P = E_b I_a$$

For constant voltage supply, $P \propto I_a$... (ii)

From (i) and (ii) $T \propto P$.

1.3 (a)

$$T = K\phi I_a$$

The value of current in series field gets halved. Hence, the armature current is to be increased in order to have fixed torque.

1.4 (b)

Since, the direction of armature current will be reversed, the nature will be cumulative. This reverse current will also change the nature of interpole flux. Hence no need to reverse the connection.

1.5 (b)

$$E_b = \frac{\phi PZN}{60A} \Rightarrow 357 = \frac{\phi \times 4 \times 51 \times 20 \times 8500}{60 \times 2}$$

$$\phi = 1.235 \text{ mWb} \approx 1.2 \text{ mWb}$$

■■■■

MADE EASY

Answers Transformers

- 2.1 (a) 2.2 (b, c) 2.3 (a) 2.4 (c) 2.5 (a) 2.6 (b) 2.7 (b)
2.8 (c)

Explanations Transformers**2.1 (a)**

Both the developed emf and current carrying capability are the functions of core area.

Current carrying capabilities or the current density of the core material is fixed. As the area has increased '4' times, current carrying capability has also increased '4' times.

The induced emf is directly proportional to core area. Hence it has also increased '4' times.

$$\text{kVA}_2 = E_2 I_2 = 4 E_1 \times 4 I_1 = 16 E_1 I_1$$

2.3 (a)

It is used to detect incipient faults.

2.4 (c)

$$W_h \propto B_m^{1.6} f$$

$$W_h \propto \frac{B_m^{1.6} f^{1.6}}{f^{0.6}} \propto \frac{V^{1.6}}{(f)^{0.6}} \quad (\text{As } V \propto B_m f)$$

$$W_e \propto B_m^2 f^2 \propto V^2$$

2.5 (a)

Since the direction of current in adjoining turns is same, it will feel force of attraction.

2.6 (b)

For satisfactory load sharing of two transformer the per unit impedances must be equal.

2.7 (b)

For half of the rated current, the voltage should be half of that voltage which will give full load current.

$$\text{i.e., } \frac{4.5 \times 11 \times 10^3}{100} = 495 \text{ V}$$

For half of the rated current,

$$V = \frac{495}{2} = 247.5 \text{ V}$$

2.8 (c)

This is a case of open delta connection which gives balanced supply voltage with reduced rating.

■■■■

- 3.1** A three-phase slip ring induction motor is fed from the rotor side with stator winding short-circuited. The frequency of the currents flowing in the short-circuited stator winding will be
 (a) slip frequency
 (b) supply frequency
 (c) frequency corresponding to rotor speed
 (d) zero
[1993 : 1 Mark]
- 3.2** Skewing is used in induction motors in order to reduce torque due to
 (a) time harmonics (b) space harmonics
 (c) slot harmonics (d) reverse rotating fields
[1994 : 1 Mark]
- 3.3** A 3-phase induction motor coupled to a pump is operating at normal speed. If one line gets disconnected, the motor stops. (State whether true or false).
[1994 : 1 Mark]
- 3.4** A six pole 50 Hz induction motor rotating at 1400 rpm is in ____ mode.
[1994 : 1 Mark]
- 3.5** In a variable frequency induction motor drive, the voltage must be varied ____ to the frequency.
[1994 : 1 Mark]
- 3.6** An induction motor runs under stable condition with constant torque load at 1250 rpm off a 50 Hz supply. Its number of poles is ____.
[1995 : 1 M]
- 3.7** When started by means of an auto transformer with 50% tapping, supply current at start of an induction motor is reduced to ____ of that when started by means of a star-delta starter.
[1995 : 2 M]

■■■■

Answers Three Phase Induction Machines

3.1 (a) **3.2** (c) **3.3** (Sol.) **3.4** (Sol.) **3.5** (Sol.) **3.6** (4) **3.7** (0.433)

Explanations Three Phase Induction Machines

3.3 Sol.

(False). Single phasing will occur but the motor will continue to run with reduced capacity.

3.4 Sol.

$$N_s = \frac{120 \times 50}{6} = 1000 \text{ rpm}$$

$$N > N_s$$

Super synchronous mode or working as an induction generator.

3.5 Sol.

Linearly,

In order to have fixed value of air gap-flux, the ratio (V/f) must be kept constant.

$$\Rightarrow \frac{V}{f} = K \Rightarrow V = Kf$$

It is directly proportional to the frequency.

3.6 Sol.

$$N_s > N \quad (\text{For stable } \theta \text{ running})$$

$$\frac{120 \times 50}{P} > 1250 \Rightarrow P < \frac{120 \times 50}{1250}$$

$$P < 4.8$$

The value of P will always be an integer nearest to this range the value is '4'.

3.7 Sol.

$$I_{\text{auto}} = (0.5)^2 \times I_{\text{sc}}$$

$$I_{Y/\Delta} = \frac{1}{\sqrt{3}} I_{\text{sc}}$$

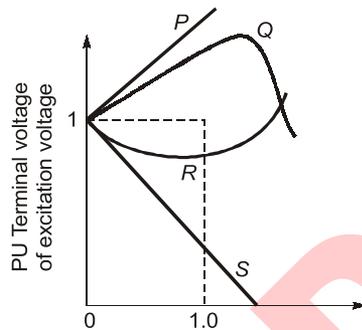
$$\frac{I_{\text{auto}}}{I_{Y/\Delta}} = (0.5)^2 \times \sqrt{3} = 0.433$$

■■■■

- 4.1 The torque angle of a synchronous machine operating from a constant voltage bus, is usually defined as the space angle between
- Rotor mmf wave and stator mmf wave
 - Rotor mmf wave & resultant flux density wave
 - Stator mmf wave & resultant flux density wave
 - Stator mmf wave and resultant mmf wave

[1992 : 1 Mark]

- 4.2 The figure, depicts the load characteristics of an isolated three-phase alternator, running at constant speed. Match the following sets of operating conditions with the given characteristics. Disregard the effects of saliency, saturation and stator resistance.



- Constant excitation and non-zero leading power-factor.
- Constant excitation & zero power-factor, leading.
- Constant terminal voltage and zero power-factor, leading.
- Constant terminal voltage and non-zero leading power-factor.

[1992 : 2 Marks]

- 4.3 A three-phase alternator has negligible stator resistance. A short-circuit test is conducted on this alternator. At a particular speed a field current of I_f is required to drive the rated armature current. If the speed of the alternator is reduced to half, the field current required to maintain rated armature current
- would be equal to I_f
 - would be equal to $2 I_f$
 - would be equal to $I_f/2$
 - cannot be predicted due to insufficient data

[1993 : 2 Marks]

- 4.4 A synchronous motor operates at 0.8 p.f. lagging. If the field current of the motor is continuously increased

- the power factor decreases upto a certain value of field current and thereafter it increases.
- the armature current increases upto a certain value of field current and thereafter it decreases.
- the power factor increases upto a certain value of field current and thereafter it decreases.
- the armature current decreases upto a certain value of field current and thereafter it increases.

From these the correct one is

- 1 and 2
- 2 and 3
- 3 and 4
- 1 and 3

[1993 : 2 Marks]

- 4.5 Two 550 kVA alternators operate in parallel to supply the following loads

- 250 kW at 0.95 power factor lag
- 100 kW at 0.8 power factor lead

One machine is supplying 200 kW at 0.9 power factor lag. The power factor of the other machine must be

- 0.89 lead
- 0.95 lead
- 0.95 lag
- 0.89 lag

[1993 : 2 Marks]

- 4.6 A synchronous motor on load draw a current at a leading power factor angle ϕ . If the internal power factor angle, which is the phase angle between the excitation emf and the current in time phasor diagram is Ψ . Then the air gap excitation mmf lags the armature mmf by

- Ψ
- $\pi/2 + \Psi$
- $\pi/2 - \Psi$
- $\Psi + \phi$

[1995 : 1 M]

- 4.7 The distribution factor for a 36 slot stator with three-phase, 8-pole winding, having 120° phase spread, is _____

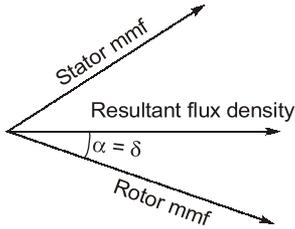
[1995 : 2 M]

Answers Synchronous Machines

4.1 (a) 4.2 (Sol.) 4.3 (a) 4.4 (c) 4.5 (a) 4.6 (c) 4.7 (0.844)

Explanations Synchronous Machines

4.1 (a)



4.2 Sol.

a - Q, b - P, c - S, d - R.

4.3 (a)

For short circuit calculation,

$$I_{sc} = \frac{E_t}{Z_s} \approx \frac{E_t}{X_s}$$

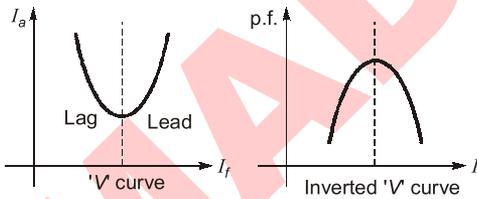
Also $E_t \propto f\phi$

and $X_s \propto f$

which gives $I_{sc} \propto \phi$

Hence short circuit current is only a function of excitation.

4.4 (c)



4.5 (a)

Total kVA supplied to load

$$= \frac{250}{0.95} \angle -\cos^{-1}(0.95)$$

$$= (250 - j82.17) \text{ kVA}$$

Total kVA supplied by M_2

$$= \frac{100}{0.8} \angle \cos^{-1}(0.8)$$

$$= 100 + j75$$

Total kVA supplied by M_1

$$= \frac{200}{0.9} \angle -\cos^{-1}(0.9)$$

$$= (200 - j96.864) \text{ kVA}$$

Using power conservation,

$$(250 - j82.17) + (100 + j75)$$

$$= (200 - j96.864) + S_2$$

$$\Rightarrow S_2 = 174.65 \angle +30.814^\circ$$

Positive signs indicates leading pf.

$$\text{p.f.} = \cos(30.814^\circ)$$

$$= 0.8588 \text{ lead.}$$

4.7 Sol.

$$m = \frac{36}{3 \times 8} = 1.5$$

$$\frac{(\text{slots/ph})}{\text{poles}} = \frac{(36/3)}{8} = \frac{12}{8} = \frac{4 \times 3}{4 \times 2}$$

Which gives $S_k = 3$

$$K_d = \frac{\sin\left(\frac{120}{2}\right)}{3 \sin\left(\frac{120}{2 \times 3}\right)} = 0.844$$



Single Phase Induction Motors, Special Purpose Machines and Electromechanical Energy Conversion Systems

- 5.1 The developed electromagnetic force and/or torque in electro-mechanical energy conversion systems act in a direction that tends
- (a) to increase the stored energy at constant mmf
 - (b) to decrease the stored energy at constant flux
 - (c) to decrease the co-energy at constant mmf
 - (d) to increase the stored energy at constant mmf
- [1992 : 1 Mark]

Answers

Single Phase Induction Motors, Special Purpose Machines and Electromechanical Energy Conversion Systems

- 5.1 (b)

Explanations

Single Phase Induction Motors, Special Purpose Machines and Electromechanical Energy Conversion Systems

- 5.1 (b)

Lenz law.



CONTENTS

1. Performance of Transmission Lines,
Line Parameters & Corona 26
2. Compensation Techniques and
Voltage Profile Control 27
3. Distribution Systems, Cables
and Insulators 28
4. Fault Analysis 29
5. Power System Stability 30
6. Switch Gear and Protection 31
7. Load Flow Studies 32
8. High Voltage DC Transmission 33

Performance of Transmission Lines, Line Parameters and Corona

- 1.1 The inductance of a power transmission line increases with
- decrease in line length.
 - increase in diameter of conductor.
 - increase in spacing between the phase conductors.
 - increase in load current carried by the conductors.
- [1992 : 1 Mark]
- 1.2 A three phase overhead transmission line has its conductors horizontally spaced with spacing between adjacent conductors equal to 'd'. If now the conductors of the line are rearranged to form an equilateral triangle of sides equal to 'd' then
- average capacitance and inductance will increase.
 - average capacitance will increase and inductance will increase.
 - average capacitance will increase and inductance will decrease.
 - surge impedance loading of the line increases.
- [1993 : 1 Mark]
- 1.3 The increase in resistance due to non-uniform distribution of current in a conductor is known as _____ effect.
- [1994 : 1 Mark]
- 1.4 The charging current of a 400 kV transmission line is more than that of a 220 kV line of the same length. [True/False]
- [1994 : 2 Marks]
- 1.5 The surge impedance of a 400 km long overhead transmission line is 400 Ω. For a 200 km length of the same line, the surge impedance will be
- 200 Ω
 - 800 Ω
 - 400 Ω
 - 100 Ω
- [1995 : 1 M]

■■■■

Answers Performance of Transmission Lines, Line Parameters and Corona

1.1 (c) 1.2 (c) 1.3 (Sol.) 1.4 (T) 1.5 (c)

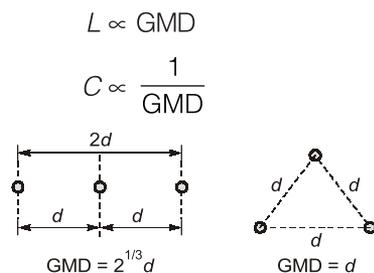
Explanations Performance of Transmission Lines, Line Parameters and Corona

1.1 (c)

$$L \propto \ln\left(\frac{d}{r'}\right)$$

$$\Rightarrow L \propto d \quad \text{and} \quad L \propto \frac{1}{r'}$$

1.2 (c)



1.3 Sol.

The increase in resistance due to non-uniform distribution of current in a conductor is known as **skin effect**.

1.4 Sol.

$$I_C = 2\pi f V_{ph} C_{ph}$$

$$I_C \propto V_{ph}$$

∴ True

1.5 (c)

Surge impedance is not a function of length of the line.

■■■■

2

Compensation Techniques and Voltage Profile Control

2.1 In a 400 kV network, 360 kV is recorded at a 400 kV bus. The reactive power absorbed by a shunt reactor rated for 50 MVAR, 400 kV connected at the bus is

- (a) 61.73 MVAR (b) 55.56 MVAR
(c) 45 MVAR (d) 40.5 MVAR

[1994 : 1 Mark]

Answers Compensation Techniques and Voltage Profile Control

2.1 (d)

Explanations Compensation Techniques and Voltage Profile Control

2.1 (d)

Reactive power absorbed,

$$Q_{\text{absorbed}} = \frac{V^2}{X_{\text{rated}}} = \frac{(360)^2}{(400)^2 / 50} = 40.5 \text{ MVAR}$$

■■■■

Distribution Systems, Cables and Insulators

3.1 The selection of size of conductors for a distributor in a distribution system is governed by

- (a) Corona loss
- (b) Temperature rise
- (c) Radio interference
- (d) Voltage drop

3.2 The insulation resistance of a cable of length 10 km is 1 MΩ. For a length of 100 km of the same cable, the insulation resistance will be ___ (in MΩ)

- (a) 1
- (b) 10
- (c) 0.1
- (d) 0.01

[1995 : 1 M]

[1992 : 1 Mark]

Answers Distribution Systems, Cables and Insulators

3.1 (d) 3.2 (c)

Explanations Compensation Techniques and Voltage Profile Control

3.2 (c)

Insulation resistance,

$$R_{\text{ins}} = \frac{\rho}{2\pi l} \ln\left(\frac{R}{r}\right) \Omega \Rightarrow \frac{R_2}{R_1} = \left(\frac{l_1}{l_2}\right)$$

$$R_2 = 1\text{M}\Omega \left(\frac{10}{100}\right) = 0.1\text{M}\Omega$$

■ ■ ■ ■

4.1 In a power-system, the 3-phase fault MVA is always higher than the single-line-ground fault MVA at a bus. (True/False).

[1994 : 1 Mark]

Answers Fault Analysis

4.1 (F)

Explanations Fault Analysis

4.1 Sol.

False. For a line to ground fault, the fault current is highest as compared to other fault conditions, given the same value of fault conditions.

■■■■

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5.1 The transient stability of the power system can be effectively improved by

- (a) improving generator excitation
- (b) phase shifting transformer
- (c) single pole switching of circuit breakers
- (d) increasing the turbine valve opening

[1993 : 1 Mark]

5.2 In a system, there are two generators operating in parallel. One generator, of rating 250 MVA, has an inertia constant of 6 MJ/MVA while the other generator of 150 MVA has an inertia constant of 4 MJ/MVA. The inertia constant for the combined system on 100 MVA common base is MJ/MVA.

[1994 : 2 Marks]

Answers Power System Stability

5.1 (c) 5.2 (21)

Explanations Power System Stability

5.1 (c)

Using high speed circuit breakers, this can be achieved.

5.2 Sol.

For 250 MVA generator

$$H = \frac{250}{100} \times 6 = 15 \text{ MJ/MVA}$$

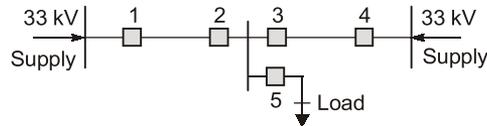
For 150 MVA generator

$$H = 4 \times \frac{150}{100} = 6 \text{ MJ/MVA}$$

$$H = 15 + 6 = 21 \text{ MJ/MVA}$$

■■■■

- 6.1 The distribution system shown in the figure is to be protected by over current system of protection. For proper fault discrimination directional over current relays will be required at locations



- (a) 1 and 4 (b) 2 and 3
(c) 1, 4 and 5 (d) 2, 3 and 5

[1993 : 2 Marks]

- 6.2 The distance relay with inherent directional property is known as _____ relay. [1995 : 1 M]
- 6.3 The inductance and capacitance of a power system network up to a circuit breaker location are 1 H and 0.01 μF respectively, the value of the shunt resistor across the circuit breaker, required for critical damping of the restriking voltage is _____.

[1995 : 1 M]

- 6.4 The insulation level of a 400 kV, EHV over head transmission line is decided on the basis of
- (a) Lightning over voltage
(b) Switching over voltage
(c) Corona inception voltage
(d) Radio and TV interference [1995 : 1 M]

- 6.5 Type of Relay most suited for
- (a) Buchholz relay (P) Feeder
(b) Translay relay (Q) Transformer
(c) Carrier current, Phase comparison relay (R) Radial distributed
(d) Directional over current relay (S) Generator
(e) Negative sequence relay (T) Ring main distributor
(U) Long overload transmission line application

[1995 : 2 M]

Answers Switch Gear and Protection

- 6.1 (b) 6.2 (Sol.) 6.3 (5) 6.4 (b) 6.5 (Sol.)

Explanations Switch Gear and Protection

6.1 (b)

If a fault occurs in between relay 1 and 2, the direction of current in relay '2' changes. Similarly if a fault occurs between relay 3 and 4 the direction of current in relay '3' changes.

Hence these relays '2' and '3' must be directional in nature.

6.2 Sol.

The distance relay with inherent directional property is known as **mho** relay.

6.3 Sol.

$$R_p = \frac{1}{2} \sqrt{\frac{L}{C}} = \frac{1}{2} \sqrt{\frac{1}{0.01 \times 10^{-6}}} = 5 \text{ k}\Omega$$

6.4 (b)

Upto 345 kV, insulation level is decided based on lightning over voltages and above 345 kV, insulation level is decided based on switching over voltage.

6.5 Sol.

- a — Q
b — P
c — U
d — T
e — S



7.1 In load flow studies of a power system, the quantities specified at a voltage controlled bus are _____ and _____.

[1992 : 1 Mark]

7.2 In load flow analysis, the load connected at a bus is represented as
 (a) constant current drawn from the bus
 (b) constant impedance connected at the bus

(c) voltage and frequency dependent source at the bus

(d) constant real and reactive power drawn from the bus

[1993 : 1 Mark]

7.3 In load-flow analysis, a voltage controlled bus is treated as a load bus in subsequent iteration for a reactive power limit is violated (True/False).

[1995 : 1 M]

Answers Load Flow Studies

7.1 (Sol.) 7.2 (d) 7.3 (T)

Explanations Load Flow Studies

7.1 Sol.

In load flow studies of a power system, the quantities specified at a voltage controlled bus are $|V|$ and P .

7.2 (d)

In load flow study generators are modeled as source of complex power, loads are modeled as demand of complex power and transmission lines are modeled as π -model.

■■■■

- 8.1 HVDC transmission is preferred to EHV – AC because
- (a) HVDC terminal equipment are inexpensive
 - (b) VAR compensation is not required in HVDC systems
 - (c) System stability can be improved
 - (d) Harmonics – problem is avoided

[1994 : 1 Mark]

Answers High Voltage DC Transmission

- 8.1 (c)

MADE EASY

Control Systems

UNIT

V

CONTENTS

1. Mathematical Models of
Physical Systems 35
2. Time Response Analysis 36
3. Concepts of Stability 37
4. Root Locus Techniques 38
5. Frequency Response Analysis 40
6. Design of Control Systems 42
7. State Variable Analysis 43

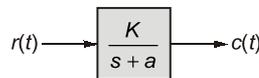
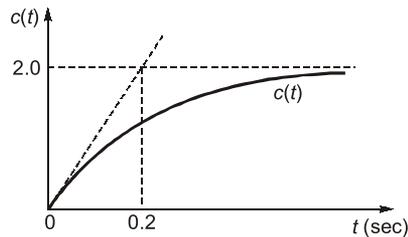
2

Time Response Analysis

2.1 A first order system and its response to a unit step input are shown in the figure below. The system parameters are

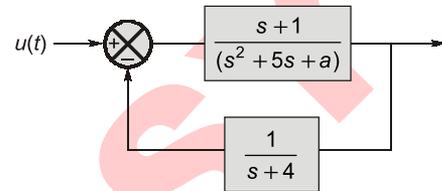
$$a = \underline{\hspace{2cm}}$$

$$K = \underline{\hspace{2cm}}$$



[1991 : 2 Marks]

2.2 For what values of 'a' does the system shown in figure have a zero steady state error [i.e. $\lim_{t \rightarrow \infty} E(t)$] for a step input?



- (a) $a = 0$ (b) $a = 2$
 (c) $a \geq 4$ (d) for no value of 'a'

[1992 : 1 Mark]

2.3 The steady state error due to a step input for type 1 system is _____. [1995 : 1 M]

Answers Time Response Analysis

2.1 (5, 10) 2.2 (a) 2.3 (0)

Explanations Time Response Analysis

2.1 (5, 10)

\therefore Time constant = 0.2 sec. (from figure)

$$= \frac{1}{a} \quad \left(\text{From } G(s) = \frac{K}{a \left(1 + \frac{s}{a} \right)} \right)$$

$$\therefore \frac{1}{a} = 0.2$$

$$\Rightarrow a = 5$$

$$\therefore \text{Final value} = \lim_{s \rightarrow 0} sC(s)$$

$$= \lim_{s \rightarrow 0} s \frac{K}{s+a} \cdot \frac{1}{s} = \frac{K}{a} = 2 \quad (\text{from figure})$$

$$\therefore \frac{K}{a} = 2$$

$$\Rightarrow K = 2 \times 5 = 10$$

2.2 (a)

$$E(s) = \frac{R(s)}{1 + G(s)H(s)}$$

$$\lim_{t \rightarrow \infty} E(t) = \lim_{s \rightarrow 0} sE(s)$$

$$= \lim_{s \rightarrow 0} \frac{s \cdot \frac{1}{s}}{1 + \frac{(s+1)}{(s^2+5s+a)} \cdot \frac{1}{(s+4)}}$$

$$\Rightarrow \frac{1}{1 + \frac{1}{4a}} = 0$$

$$\Rightarrow \frac{4a}{4a+1} = 0$$

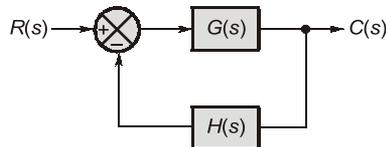
$$\text{Hence, } a = 0$$

2.3 (0)

$$\lim_{s \rightarrow 0} sE(s) = \lim_{s \rightarrow 0} \frac{s \cdot \frac{1}{s}}{1 + \frac{G'(s)H(s)}{s}} = 0$$



- 3.1 The closed loop system of figure is stable if the transfer function $T(s) = \frac{C(s)}{R(s)}$ is stable. (True/False)



[1994 : 1 Mark]

- 3.2 The number of positive real roots of the equation $s^3 - 2s + 2 = 0$ is _____.

[1994 : 1 Mark]

- 3.3 Closed loop stability implies that $[1 + G(s)H(s)]$ has all the _____ in the left half of the s-plane.

[1995 : 1 M]

Answers Concepts of Stability

3.1 (Sol.) 3.2 (Sol.) 3.3 (Sol.)

Explanations Concepts of Stability

3.1 Sol.

All the close loop poles must lie in left half of the s-plane.

3.2 Sol.

$$\therefore s^3 - 2s + 2 = 0$$

$$\therefore s = -1.77, 0.88 \pm j0.59$$

Hence, no positive real root exists.

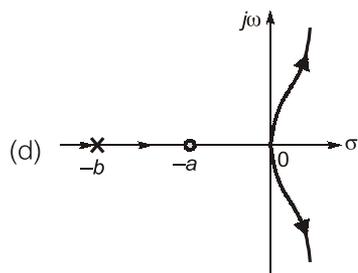
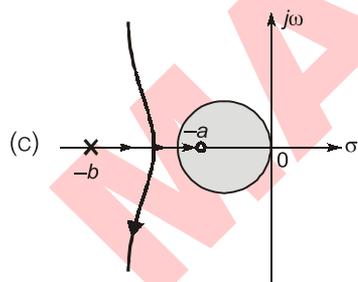
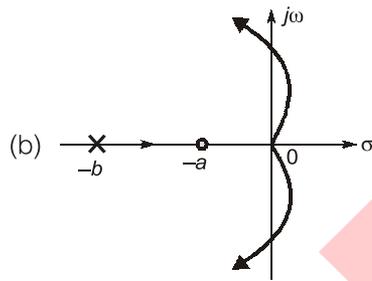
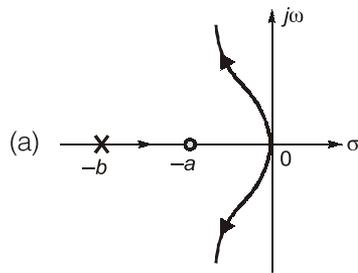
■■■■

4

Root Locus Techniques

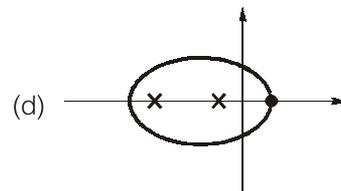
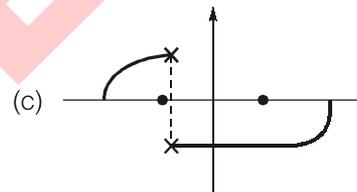
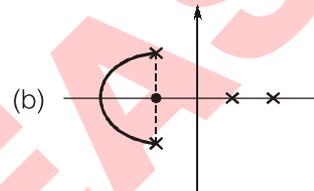
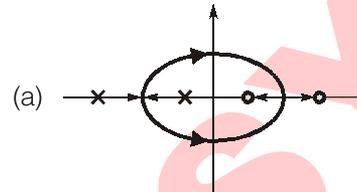
4.1 A unity feedback system has an open loop transfer function of the form $KG(s) = \frac{K(s+a)}{s^2(s+b)}$; $b > a$

which of the loci shown in the figure can be valid root-loci for the system?



[1991 : 1 Mark]

4.2 Which of the following figure(s) represent valid root loci in the s-plane for positive K ? Assume that the system has transfer function with real coefficient.



[1992 : 1 Mark]

Answers Root Locus Techniques

4.1 (a) 4.2 (a)

Explanations Root Locus Techniques**4.1 (a)**

$$P = 3, \quad Z = 1$$

and two repeating poles at origin

$$\begin{aligned} \text{Centroid} &= \frac{0 - b - (-a)}{3 - 1} \\ &= \frac{-(b - a)}{2} < 0 \end{aligned}$$

$$\begin{aligned} \text{Angle of asymptotes} &= \frac{(2q + 1) 180^\circ}{3 - 1} \\ &= 90^\circ \quad (\text{for } q = 0) \\ &= 270^\circ \quad (\text{for } q = 1) \end{aligned}$$

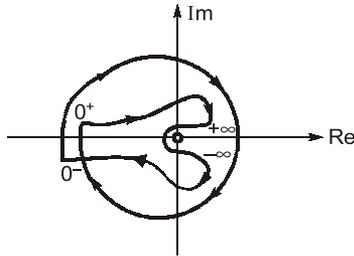
 \therefore Option (a) is correct.**4.2 (a)**

The valid root loci in the s-plane can be only option (a), because of symmetry and root locus definition.



MADE EASY

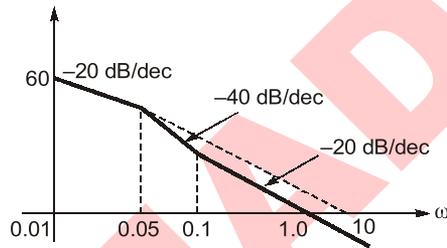
5.1 Which of the following is the transfer function of a system having the Nyquist plot shown in the figure below?



- (a) $\frac{K}{s(s+2)^2(s+5)}$ (b) $\frac{K}{s^2(s+2)(s+5)}$
 (c) $\frac{K(s+1)}{s^2(s+2)(s+5)}$ (d) $\frac{K(s+1)(s+3)}{s^2(s+2)(s+5)}$

[1991 : 1 Mark]

5.2 The system having the Bode magnitude plot shown in the figure below has the transfer function.



- (a) $\frac{60(s+0.01)(s+0.1)}{s^2(s+0.05)^2}$
 (b) $\frac{10(1+10s)}{s(1+20s)}$
 (c) $\frac{3(s+0.05)}{s(s+0.1)(s+1)}$
 (d) $\frac{5(s+0.1)}{s(s+0.05)}$

[1991 : 1 Mark]

5.3 A unity feedback system has the open loop transfer function,

$$G(s) = \frac{1}{(s-1)(s+2)(s+3)}$$

The Nyquist plot of $G(s)$ encircle the origin.

- (a) Never (b) Once
 (c) Twice (d) Thrice

[1992 : 1 Mark]



Answers **Frequency Response Analysis**

- 5.1 (b) 5.2 (b, d) 5.3 (a)

Explanations Frequency Response Analysis**5.1 (b)**

∴ Curve starts from $-180^\circ \Rightarrow$ type 2 system and
 ∴ Curve ends at -360° .
 \Rightarrow difference between number of poles and
 number of zeros = $\frac{360^\circ}{90^\circ} = 4$
 ∴ Only option (b) is satisfying these two
 properties, So, option (b) is correct.

5.2 (b, d)

Type = 1

Poles at $\Rightarrow \omega = 0, 0.05$ Zero at $\Rightarrow \omega = 0.1$

Using initial line equation,

$$\text{dB} = 20 \log K - 20 \log(\omega)$$

At $\omega = 0.01$

$$\text{dB} = 60$$

$$\therefore 60 = -20 \log(0.01) + 20 \log K$$

On solving, $K = 10$

Therefore,

$$\text{Transfer function} = \frac{10(1+10s)}{s(1+20s)} = \frac{5(s+0.1)}{s(s+0.05)}$$

5.3 (a)

$$G(s) = \frac{1}{(s-1)(s+2)(s+3)}$$

$$1 + G(s)H(s) = 0$$

$$\text{i.e., } s^3 + 4s^2 + s - 5 = 0$$

Applying Routh criteria

s^3	1	1
s^2	4	-5
s^1	9/4	0
s^0	-5	

Hence, number of closed loop poles at RHS of
 s-plane = number of sign changes = One.

Number of encirclements of $G(s)$ about origin
 = Number of encirclements of $G(s)H(s)$ about
 $(-1, 0) = \{\text{Number of open loop poles at RHS of
 s-plane} - \text{Number of closed loop poles at RHS of
 s-plane}\}.$

$$N = P - Z = 1 - 1 = 0$$

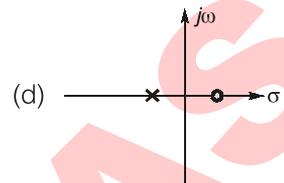
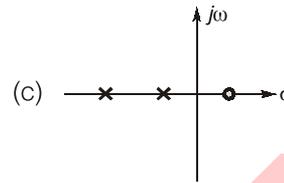
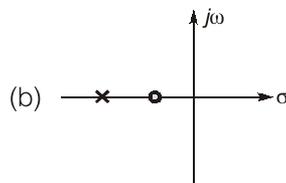
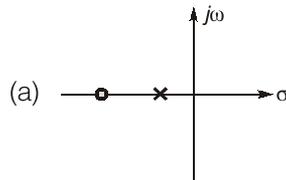
∴ No encirclement of origin of $G(s)$.

■■■■

6

Design of Control Systems

6.1 The pole zero configuration of a phase lead compensator is given by



[1994 : 1 Mark]

Answers Design of Control Systems

6.1 (b)

Explanations Design of Control Systems

6.1 (b)

In phase lead compensator $|P| > |Z|$.

■■■■

7.1 The transfer function for the state variable representation $\dot{X} = AX + BU$, $Y = CX + DU$, is given by

- (a) $D + C(sI - A)^{-1} B$
 (b) $B(sI - A)^{-1} C + D$
 (c) $D(sI - A)^{-1} B + C$
 (d) $C(sI - A)^{-1} D + B$

[1993 : 1 Mark]

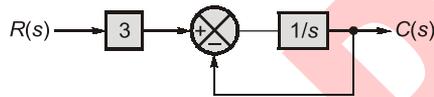
7.2 Consider a second order system whose state space representation is of the form $\dot{X} = AX + BU$.

If $x_1(t) = x_2(t)$, then system is

- (a) controllable (b) uncontrollable
 (c) observable (d) unstable

[1993 : 1 Mark]

7.3 The matrix of any state space equations for the transfer function $C(s)/R(s)$ of the system, shown below in the figure is



- (a) $\begin{pmatrix} -1 & 0 \\ 0 & 1 \end{pmatrix}$ (b) $\begin{pmatrix} 1 & 0 \\ 0 & -1 \end{pmatrix}$
 (c) $[-1]$ (d) $[3]$

[1994 : 1 Mark]

7.4 The eigen-values of the matrix $\begin{bmatrix} a & 1 \\ a & 1 \end{bmatrix}$ are

- (a) $(a + 1), 0$ (b) $a, 0$
 (c) $(a - 1), 0$ (d) $0, 0$

[1994 : 1 Mark]

7.5 A system is described by the state equation $\dot{X} = AX + BU$. The output is given by $Y = CX$.

Where, $A = \begin{pmatrix} -4 & -1 \\ 3 & -1 \end{pmatrix}$, $B = \begin{pmatrix} 1 \\ 1 \end{pmatrix}$, $C = [1 \ 0]$.

Transfer function $G(s)$ of the system is

- (a) $\frac{s}{s^2 + 5s + 7}$ (b) $\frac{1}{s^2 + 5s + 7}$
 (c) $\frac{s}{s^2 + 3s + 2}$ (d) $\frac{1}{s^2 + 3s + 2}$

[1995 : 1 M]

7.6 Given the matrix: $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -6 & -11 & -6 \end{bmatrix}$

Its eigen values are _____ [1995 : 1 M]

■■■■

Answers State Variable Analysis

7.1 (a) 7.2 (b) 7.3 (c) 7.4 (a) 7.5 (a) 7.6 (-1, -2, -3)

Explanations State Variable Analysis**7.1 (a)**

$$\text{T.F.} = C[sI - A]^{-1} B + D$$

7.2 (b)

$$\text{Let, } \begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} a & b \\ c & d \end{bmatrix} \begin{bmatrix} x_1(t) \\ x_2(t) \end{bmatrix} + \begin{bmatrix} e \\ f \end{bmatrix} u(t)$$

$$[B] = \begin{bmatrix} e \\ f \end{bmatrix}, \quad [AB] = \begin{bmatrix} ae + bf \\ ce + df \end{bmatrix}$$

Since, $x_1(t) = x_2(t)$ and $\dot{x}_1(t) = \dot{x}_2(t)$

$$\Rightarrow e = f \text{ and } a + b = c + d$$

$$\therefore |Q_d| = |B \ AB| = \begin{vmatrix} e & ae + bf \\ f & ce + df \end{vmatrix} = 0$$

\Rightarrow Uncontrollable.

7.3 (c)

$$\text{T.F.} = \frac{3}{s+1}$$

\Rightarrow Pole = -1

\therefore Eigen value of 'A' = -1

\Rightarrow Option (c) is correct.

7.4 (a)

Characteristic equation:

$$|sI - A| = 0$$

$$\begin{vmatrix} s-a & -1 \\ -a & s-1 \end{vmatrix} = 0$$

$$(s-a)(s-1) - a = 0$$

\therefore Eigen values, $s = 0, (a+1)$

7.5 (a)

$$\text{T.F.} = C[sI - A]^{-1} B + D$$

$$= [1 \ 0] \cdot \begin{bmatrix} s+4 & 1 \\ -3 & s+1 \end{bmatrix}^{-1} \cdot \begin{bmatrix} 1 \\ 1 \end{bmatrix} + 0$$

$$= \frac{[1 \ 0] \cdot \begin{bmatrix} s+1 & -1 \\ 3 & s+4 \end{bmatrix} \cdot \begin{bmatrix} 1 \\ 1 \end{bmatrix}}{(s+1)(s+4) + 3}$$

$$= \frac{[s+1 \ -1] \cdot \begin{bmatrix} 1 \\ 1 \end{bmatrix}}{s^2 + 5s + 4 + 3} = \frac{s}{s^2 + 5s + 7}$$

7.6 (-1, -2, -3)

$$|sI - A| = \begin{vmatrix} s & -1 & 0 \\ 0 & s & -1 \\ 6 & 11 & s+6 \end{vmatrix} = 0$$

$$s^3 + 6s^2 + 11s + 6 = 0$$

\therefore Eigen values are $s = -1, -2, -3$.

■■■■

Electrical & Electronic Measurements

UNIT VI

CONTENTS

1. Characteristics of Instruments and Measurement Systems 46
2. Galvanometers, Voltmeters and Ammeters 47
3. Measurement of Resistance and Potentiometers 49
4. Measurement of Energy and Power 50
5. CRO and Electronic Measurements 51

Characteristics of Instruments and Measurement Systems

1.1 A precise measurement guarantees accuracy of the measured quantity. (True/False).

[1994 : 1 Mark]

1.2 Four ammeters M1, M2, M3 and M4 with the following specifications are available.

Instrument	Type	Full scale value (A)	Accuracy % of FS
M1	$3\frac{1}{2}$ digit dual slope	20	± 0.10
M2	PMMC	10	± 0.20
M3	Electro-dynamic	5	± 0.50
M4	Moving-iron	1	± 1.00

A current of 1 A is to be measured. To obtain minimum error in the reading, one should select meter

(a) M1

(b) M2

(c) M3

(d) M4

[1995 : 1 M]

Answers Characteristics of Instruments and Measurement Systems

1.1 (Sol.) 1.2 (d)

Explanations Characteristics of Instruments and Measurement Systems

1.1 Sol.

Preciseness means repeatability of readings it does not guarantees the accuracy.

1.2 (d)

Error in reading of first meter

$$= \text{FSD} \times \text{accuracy} = 20 \times \frac{\pm 0.1}{100} = \pm 0.02$$

Error in reading of second meter

$$= 10 \times \frac{\pm 0.2}{100} = \pm 0.02$$

Error in reading of third meter

$$= 5 \times \frac{\pm 0.5}{100} = \pm 0.025$$

Error in reading of fourth meter

$$= 1 \times \frac{\pm 1.00}{100} = \pm 0.01$$

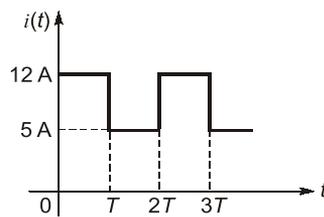
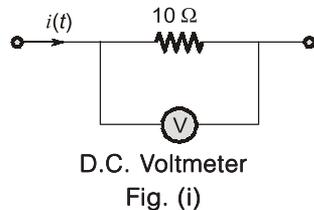
Fourth meter has least error.



2

Galvanometers, Voltmeters and Ammeters

- 2.1 The current $i(t)$ passing through $10\ \Omega$ resistor as shown in the Fig. (i) as a waveform as shown in Fig. (ii). Then the reading of the DC voltmeter is connected across $10\ \Omega$ resistor is



[1991 : 1 Mark]

- 2.2 An unshielded moving iron voltmeter is used to measure the voltage in an ac circuit. If a stray DC magnetic field having a component along the axis of the meter coil appears, the meter reading would be
- unaffected
 - decreased
 - increased

- (d) either decreased or increased depending on the direction of the DC field

[1992 : 1 Mark]

- 2.3 A metal strain gauge has factor of two. Its nominal resistance is $120\ \text{ohms}$. It undergoes a strain of 10^{-5} , the value of change of resistance in response to the strain is
- $240\ \text{ohms}$
 - $2 \times 10^{-5}\ \text{ohms}$
 - $2.4 \times 10^{-3}\ \text{ohms}$
 - $1.2 \times 10^{-3}\ \text{ohms}$

[1993 : 1 Mark]

- 2.4 A 0-10 mA PMMC ammeter reads 4 mA in a circuit. Its bottom control spring snaps suddenly. The meter will now read nearly
- 10 mA
 - 8 mA
 - 2 mA
 - zero

[1994 : 1 Mark]

- 2.5 Two 100 V full scale PMMC type dc voltmeter having figure of merits (FOM) of $10\ \text{k}\Omega/\text{V}$ and $20\ \text{k}\Omega/\text{V}$ are connected in series. The series combination can be used to measure a maximum DC voltage of ____ V.

[1995 : 1 M]

Answers Galvanometers, Voltmeters and Ammeters

2.1 (85) 2.2 (d) 2.3 (c) 2.4 (d) 2.5 (150)

Explanations Galvanometers, Voltmeters and Ammeters

2.1 Sol.

The voltmeter will read average value,

$$I_{av} = \left(\frac{12+5}{2} \right) \text{A}$$

$$V = I_{av} \times 10\ \Omega = \left(\frac{12+5}{2} \right) \times 10 = 85$$

2.2 (d)

Since, magnetic field is a vector quantity, direction is to be specified.

2.3 (c)

$$G = \frac{\Delta R / R}{\Delta l / l}$$

$$\Rightarrow \frac{\Delta R}{R} = 2 \times 10^{-5}$$

$$\Delta R = 120 \times 2 \times 10^{-5}\ \Omega$$

$$= 2.4 \times 10^{-3}\ \Omega$$

2.4 (d)

The current through coil will be zero, because in PMMC type instruments control spring is connected in series with the moving coil.

2.5 Sol.

$$(I_{fsc})_1 = \frac{1}{10 \text{ k}\Omega/\text{V}} = 0.05 \text{ mA}$$

$$(I_{fsc})_2 = \frac{1}{20 \text{ k}\Omega/\text{V}} = 0.05 \text{ mA}$$

In series application, maximum current will be 0.05 mA

Resistance of $M_1 = 10 \text{ k}\Omega/\text{V} \times 100 \text{ V} = 1 \text{ M}\Omega$

Resistance of $M_2 = 20 \text{ k}\Omega/\text{V} \times 100 \text{ V} = 2 \text{ M}\Omega$

Hence, the maximum voltage rating

$$= I_{\max} \cdot (R_{M_1} + R_{M_2})$$

$$= 0.05 \text{ mA} \times (1 + 2) \text{ M}\Omega = 150 \text{ V}$$

■■■■

MADE EASY

3

Measurement of Resistance and Potentiometers

- 3.1 In DC potentiometer measurements, a second reading is often taken after reversing the polarities of the DC supply and the unknown voltage, and the average of the two readings is taken. This is done with a view to eliminate the effects of
- (a) ripples in the DC supply
 - (b) stray magnetic fields
 - (c) stray thermal emf's
 - (d) erroneous standardization

[1992 : 1 Mark]

- 3.2 A DC potentiometer is designed to measure up to 2 V with a slide wire of 800 mm. A standard cell of emf 1.18 V obtains balance at 600 mm. A test cell is seen to obtain balance at 680 mm. The emf of the test cell is
- (a) 1.00 V
 - (b) 1.34 V
 - (c) 1.50 V
 - (d) 1.70 V

[1994 : 2 Marks]

- 3.3 A Kelvin double bridge is best suited for the measurement of
- (a) inductance
 - (b) capacitance
 - (c) low resistance
 - (d) high resistance

[1995 : 1 M]

Answers Measurement of Resistance and Potentiometers

3.1 (c) 3.2 (b) 3.3 (c)

Explanations Measurement of Resistance and Potentiometers

3.2 (b)

∴ Balance at 600 mm is corresponding to an emf of 1.18 V.

∴ Balance at 680 mm is corresponding to an emf

$$\text{of } \frac{1.18}{600} \times 680 \approx 1.34 \text{ V.}$$

3.3 (c)

It is used for the measurement of low resistance.

■■■■

4

Measurement of Energy and Power

- 4.1 The voltage phasor of a circuit is $10\angle 15^\circ$ V and the current phasor is $2\angle -45^\circ$ A. The active and the reactive powers in the circuit are
- (a) 10 W and 17.32 VAR
 - (b) 5 W and 8.66 VAR
 - (c) 20 W and 60 VAR
 - (d) $20\sqrt{2}$ W and $10\sqrt{2}$ VAR

[1994 : 2 Marks]

Answers Measurement of Energy and Power

4.1 (a)

Explanations Measurement of Energy and Power

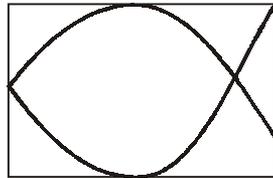
4.1 (a)

$$\begin{aligned}\text{Complex power} &= VI^* \\ &= 10\angle 15^\circ \times 2\angle 45^\circ = 20\angle 60^\circ \\ &= (10 + j10\sqrt{3}) \\ &= (10 + j17.32) = P + jQ \\ \Rightarrow P &= 10 \text{ W and } Q = 17.32 \text{ VAR}\end{aligned}$$

■■■■

CRO and Electronic Measurements

5.1 A lissajous pattern, as shown in the figure below, is observed on the screen of a CRO when voltages of frequencies f_x and f_y are applied to be x and y plates respectively. $f_x : f_y$ is then equal to



- (a) 3 : 2 (b) 1 : 2
(c) 2 : 3 (d) 2 : 1

[1994 : 1 Mark]

5.2 A certain oscilloscope with 4 cm screen has its own sweep output fed to its input. If the x and y sensitivities are same, the oscilloscope will display a

- (a) triangular wave (b) diagonal line
(c) sine wave (d) circle [1995 : 1 M]

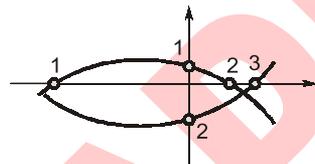
Answers CRO and Electronic Measurements

5.1 (c) 5.2 (b)

Explanations CRO and Electronic Measurements

5.1 (c)

$$\frac{f_x}{f_y} = \frac{2}{3}$$



5.2 (b)

- \therefore x and y sensitivities are same.
 \therefore Deflection by both will be same.

■■■■

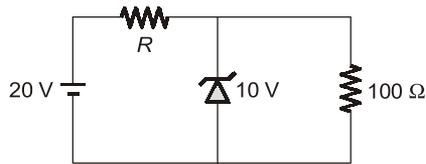
Analog Electronics

UNIT VII

CONTENTS

1. Diodes and their Applications 53
2. BJT, FET and their Biasing Circuits 54
3. Operational Amplifiers 55
4. Oscillators and Feedback Amplifiers 57

- 1.1 The figure shows an electronic voltage regulator. The zener diode may be assumed to require a minimum current of 25 mA for satisfactory operations. The value of R required for satisfactory voltage regulation of the circuit is



[1991 : 2 Marks]

Answers Diodes and their Applications

1.1 (80)

Explanations Diodes and their Applications

1.1 (80)

Current in $100\ \Omega$ resistance

$$I_{100} = \frac{10\text{ V}}{100\ \Omega} = 100\text{ mA}$$

$$I_2 = 25\text{ mA}$$

$$\begin{aligned} \text{Current in resistance } R, &= 100\text{ mA} + 25\text{ mA} \\ &= 125\text{ mA} \end{aligned}$$

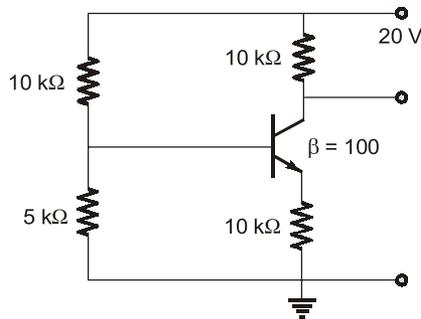
$$\text{Also, } 20 - 10 = 125 \times 10^{-3} \times R$$

$$R = \frac{10 \times 1000}{125} = 80\ \Omega$$

■■■■

BJT, FET and their Biasing Circuits

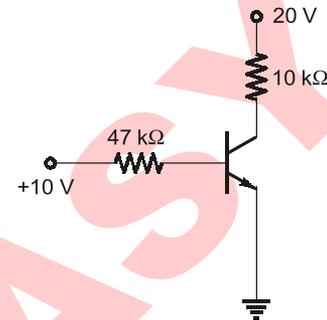
2.1 The figure shown below, shows a common emitter amplifier. The quiescent collector voltage of the circuit is approximately



- (a) $\frac{20}{3}$ V (b) 10 V
 (c) 14 V (d) 20 V

[1991 : 1 Mark]

2.2 In the transistor circuit shown in the figure. Collector to ground voltage is +20 V. Which of the following is the probable cause of error?



- (a) Collector emitter terminals shorted
 (b) Emitter to ground connection open
 (c) 10 kΩ resistor open
 (d) Collector base terminals shorted

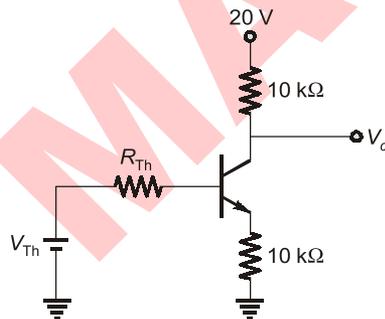
[1994 : 1 Mark]

Answers BJT, FET and their Biasing Circuits

2.1 (c) 2.2 (b)

Explanations BJT, FET and their Biasing Circuits

2.1 (c)



$$V_{Th} = \frac{5}{15} \times 20 \text{ V} = 6.67 \text{ V}$$

$$R_{Th} = \frac{10 \times 5}{10 + 5} = 3.33 \text{ } \Omega$$

$$V_{Th} - I_b R_{Th} - 0.7 - (\beta + 1)I_b \times 10 \text{ k}\Omega = 0$$

$$5.97 = I_b(3.33 + 101 \times 10) \text{ k}\Omega$$

$$I_b = 5.891 \text{ } \mu\text{A}$$

$$I_c = \beta I_b = 0.589 \text{ mA}$$

$$V_c = 20 - 10 \times I_c$$

$$= 14.11 \text{ V} \approx 14 \text{ V}$$

2.2 (b)

$$20 - 10 \text{ k} \times I_c = 20$$

$$\Rightarrow I_c = 0 \text{ which gives}$$

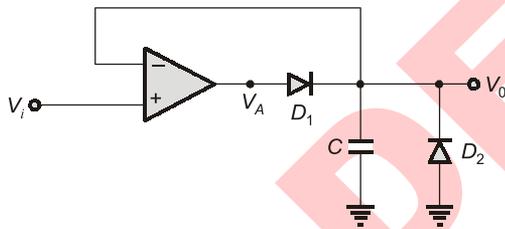
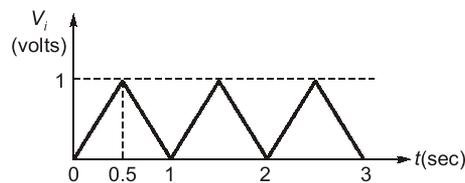
$$I_E = I_C = I_B = 0$$

That is only possible when emitter connection is open. In other cases there will be base current.

- 3.1 An ideal op-amp is used to make an inverting amplifier. The two input terminals of the op-amp are at the same potential because
- the two input terminals are directly shorted internally.
 - the input impedance of the op-amp is infinity.
 - the open-loop gain of the op-amp is infinity.
 - CMRR is infinity.

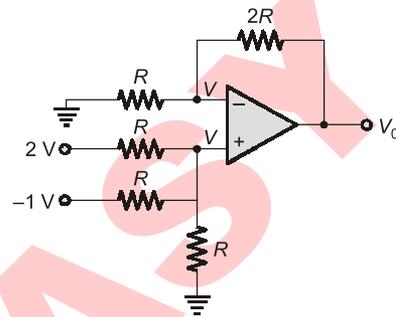
[1992 : 1 Mark]

- 3.2 The circuit shown in the figure is excited by the input wave form shown. Sketch the wave form of the output. Assume all the components are ideal.



[1992 : 2 Marks]

- 3.3 Given figure, shows a non-inverting op-amp summer with $V_1 = 2\text{ V}$ and $V_2 = -1\text{ V}$ the output voltage $V_0 =$ _____.



[1994 : 1 Mark]

- 3.4 The common mode voltage of a unity gain (voltage follower) op-amp buffer in terms of its output voltage V is _____.

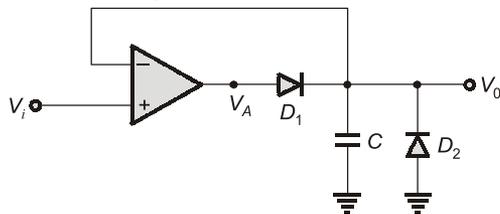
[1995 : 1 M]

Answers Operational Amplifiers

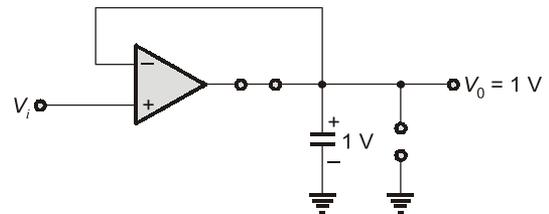
3.1 (c, d) 3.2 (Sol.) 3.3 (1) 3.4 (Sol.)

Explanations Operational Amplifiers

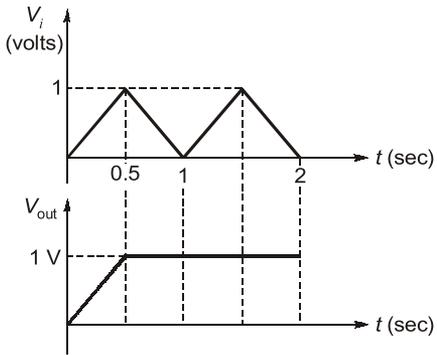
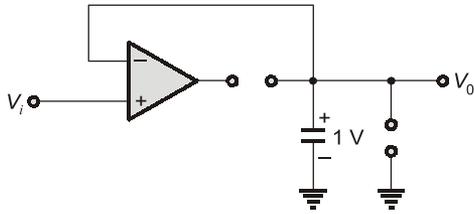
3.2 Sol.



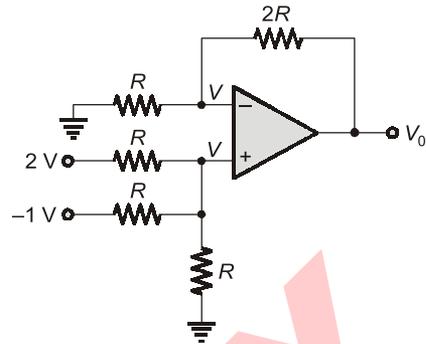
For $0 < t < 0.5\text{ s}$
Capacitor get charged upto 1 volt. D_1 is forward bias and D_2 is reversed bias.



There is no discharging path provided for this capacitor. It will remain charged with 1 V.



3.3 (1)



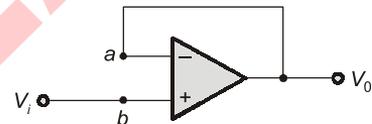
$$\frac{2-V}{R} + \frac{-1-V}{R} = \frac{V}{R}$$

$$\Rightarrow V = \frac{1}{3} \text{ Volts}$$

$$\frac{0-V}{R} = \frac{V-V_0}{2R}$$

$$V_0 = 3V = 1 \text{ Volt}$$

3.4 Sol.



Here, $V_i = V_0$

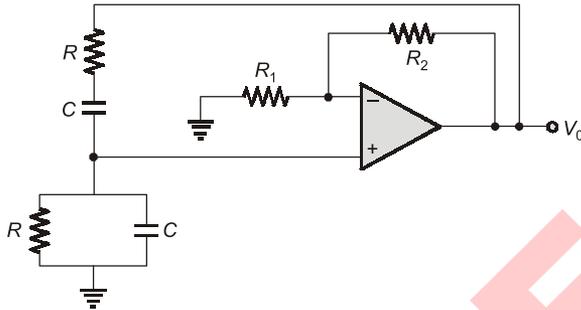
$$V_{cm} = V_a + V_b = \frac{1}{2}(V_i + V_0) = V_i = V_0$$

■■■■

- 4.1 In a common emitter amplifier, the unbypassed emitter resistance provides
- voltage-shunt feedback
 - current-series feedback
 - negative-voltage feedback
 - positive-current feedback

[1992 : 1 Mark]

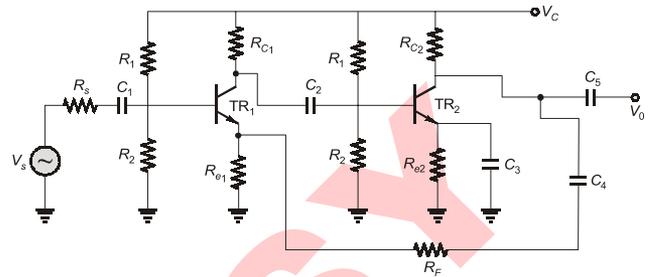
- 4.2 A Wein bridge oscillator is shown in figure. Which of the following statements are true, if 'f' is the frequency of oscillation?



- For $R = 1 \text{ k}\Omega$, $C = \frac{1}{2\pi} \mu\text{F}$, $f = 1 \text{ kHz}$
- For $R = 3 \text{ k}\Omega$, $C = \frac{1}{18\pi} \mu\text{F}$, $f = 3 \text{ kHz}$
- The gain of the op-amp stage should be less than two for proper operation.
- The gain of op-amp should be three for proper operation.

[1993 : 1 Mark]

- 4.3 Given figure shows a two stage small signal transistor feedback amplifier. Match the defective component (listed on the left hand side below) with its probable effect on the circuit (listed on the right hand side).



List-I

- Capacitor C_1 is open
- Capacitor C_3 is open
- Capacitor C_4 is open
- R_{C2} is shorted

List-II

- All DC voltages normal, V_0 increase marginally.
- Collector of TR_2 at V_{CC} , $V_0 = 0$.
- All DC voltages normal, gain of 2nd stage decrease V_0 decrease.
- All DC voltage normal, $V_0 = 0$.
- All DC voltage normal, overall gain of the amplifier increases, V_0 increase.
- No change

[1994 : 1 Mark]

- 4.4 A practical RC sinusoidal oscillator is built using a positive feedback amplifier with a closed loop gain slightly less than unity. (True/False)

[1994 : 1 Mark]



Answers Oscillators and Feedback Amplifiers

4.1 (b) 4.2 (a,b,d) 4.3 (Sol.) 4.4 (F)

Explanations Oscillators and Feedback Amplifiers**4.3 Sol.** $A \rightarrow S, B \rightarrow R, C \rightarrow T, D \rightarrow Q.$ **4.4 Sol.**

False.

■■■■

MADE EASY

Digital Electronics

UNIT VIII

CONTENTS

1. Sequential Logic Circuits 60
2. A/D and D/A Converters 61
3. Microprocessors 62

MADE

1

Sequential Logic Circuits

- 1.1 For a J-K flip-flop, J input is tied to its own \bar{Q} output and its K input is connected to its own Q output. If the flip-flop is fed with a clock of frequency 1 MHz, its Q output frequency will be _____.
[1995 : 1 M]

Answers Sequential Logic Circuits

1.1 (0.5)

Explanations A/D and D/A Converters

1.1 (0.5)

$$f_{\text{out}} = \frac{f_{\text{in}}}{2} = \frac{1\text{MHz}}{2} = 0.5\text{MHz}$$

■■■■

MADE EASY

2

A/D and D/A Converters

2.1 A 10 bit A/D converter is used to digitize an analog signal in the 0 to 5 V range. The maximum peak to peak ripple voltage that can be allowed in the DC supply voltage is

- (a) nearly 100 mV (b) nearly 50 mV
(c) nearly 25 mV (d) nearly 5 mV

[1993 : 1 Mark]

2.2 The number of comparisons carried out in a 4-bit flash-type A/D converter is

- (a) 16 (b) 15
(c) 4 (d) 3 [1994 : 1 Mark]

Answers A/D and D/A Converters

2.1 (d) 2.2 (b)

Explanations A/D and D/A Converters

2.1 (d)

If the ripple voltage is more than the resolution, it will go to next level.

$$\text{Resolution} = \frac{V}{2^n} = \frac{5}{2^{10}} \simeq 5 \text{ mV}$$

2.2 (b)

Number of comparators
 $= 2^N - 1 = 2^4 - 1 = 15$

■■■■

- 3.1** If the *HLT* instruction of a 8085 microprocessor is executed
- the microprocessor is disconnected from the system bus till the reset is pressed.
 - the microprocessor enters into a halt state and the buses are tri-stated.
 - the microprocessor halts execution of the program and returns to monitor.
 - the microprocessor reloads the program from the locations 0024 and 0025H.

[1992 : 1 Mark]

- 3.2** Three devices *A*, *B* and *C* have to be connected to a 8085 microprocessor. Device *A* has highest priority and device *C* has the lowest priority. In this context which of the statements are correct?
- A* uses TRAP, *B* uses RST 5.5 and *C* uses RST6.5.
 - A* uses RST 7.5, *B* uses RST 6.5 and *C* uses RST 5.5.
 - A* uses RST 5.5, *B* uses RST 6.5 and *C* uses RST 7.5.
 - A* uses RST 5.5, *B* uses RST 6.5 and *C* uses TRAP.

[1993 : 1 Mark]

- 3.3** The contents of the accumulator in an 8085 microprocessor is altered after the execution of the instruction

- CMP *C*
- CPI 3A
- ANI 5C
- ORA *A*

[1994 : 1 Mark]

- 3.4** The stack pointer of a microprocessor is at A001. At the end of execution of following instructions, the value of stack pointer is _____

```
PUSH PSW
XTHL
PUSH D
JMP FC70H
```

[1994 : 2 Marks]

- 3.5** In an 8085 microprocessor, after the execution of XRA *A* instruction

- the carry flag is set.
- the accumulator contain FFH.
- the zero flag is set.
- the accumulator contents are shifted left by one bit.

[1995 : 1 M]

Answers Microprocessors

3.1 (b) 3.2 (b) 3.3 (c) 3.4 (Sol.) 3.5 (c)

Explanations Microprocessors

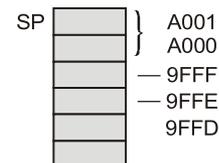
3.2 (b)

Priority order.
TRAP > RST 7.5 > RST 6.5 > RST 5.5 > INTR.

3.3 (c)

Compare instruction does not alter the content accumulator. Similarly self OR operation will also not alter the content of accumulator.

3.4 Sol.



```
A 0 0 1 H
  0 4 H
  ---
 9 F F 0 H
```

3.5 (c)

Accumulator gets cleared.



Power Electronics

UNIT IX

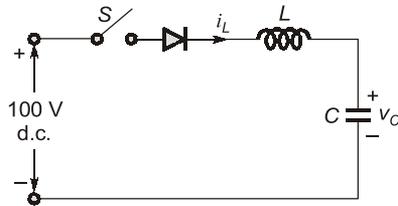
CONTENTS

1. Power Semiconductor Devices and
Commutation Techniques 64
2. Phase Controlled Rectifiers 65
3. Choppers 66
4. Inverters 67
5. Miscellaneous 68

MA

Power Semiconductor Devices and Commutation Techniques

1.1 In the circuit of figure the switch 'S' is closed at $t = 0$ with $i_L(0) = 0$ and $v_C(0) = 0$. In the steady state v_C equals



- (a) 200 V (b) 100 V
(c) zero (d) -100 V

[1992 : 1 Mark]

1.2 The thermal resistance between the body of a power semiconductor device and the ambient is expressed as

- (a) voltage across the device divided by current through the device.
(b) average power dissipated in the device divided by the square of the rms current in the device.
(c) average power dissipated in the device divided by the temperature difference from body to ambient.

(d) temperature difference from body to ambient divided by average power dissipated in the device.

[1993 : 1 Mark]

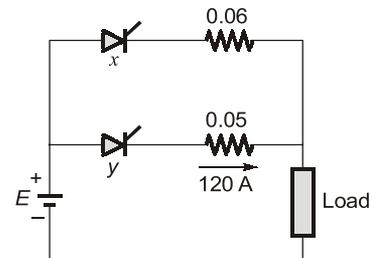
1.3 A triac can be triggered by a gate pulse of _____ polarity. [1994 : 1 Mark]

1.4 A switched mode power supply operating at 20 kHz to 100 kHz range uses as the main switching element.

- (a) Thyristor (b) MOSFET
(c) Triac (d) UJT

[1994 : 1 Mark]

1.5 The figure show two thyristors, each rated 500 A (continuous) sharing a load current. Current through thyristor y is 120 A. The current through thyristor x will be nearly _____ A



[1995 : 1 M]

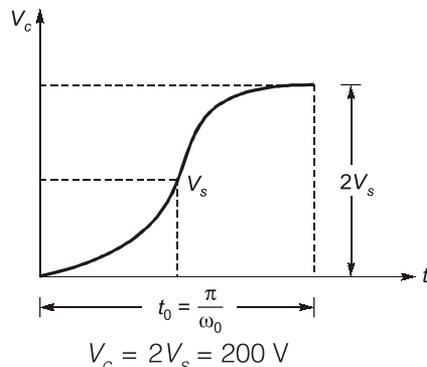
Answers Power Semiconductor Devices & Commutation Techniques

1.1 (a) 1.2 (d) 1.3 (+ve, -ve) 1.4 (b) 1.1 (100)

Explanations Power Semiconductor Devices & Commutation Techniques

1.1 (a)

Voltage across capacitor,



1.3 Sol.

Both positive and negative.

1.4 (b)

MOSFET is used for this frequency range.

1.5 Sol.

Since both the thyristors are working in parallel, the voltage difference will be same.

$$120 \times 0.05 = I_x \times 0.06 \Rightarrow I_x = \frac{120 \times 5}{6} = 100 \text{ A}$$

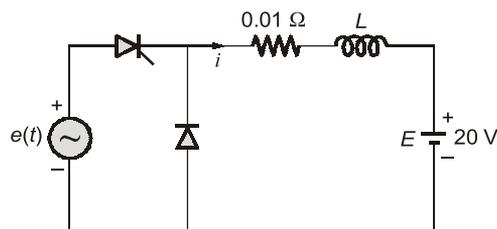


2

Phase Controlled Rectifiers

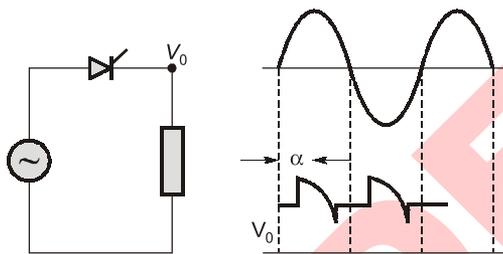
2.1 In the circuit shown in the figure, L is large and the average value of 'i' is 100 A. The thyristor is gated in the _____ half cycle of 'e' at a delay angle is equal to _____

$$e(t) = 200\sqrt{2} \sin 314t.$$



[1992 : 1 Mark]

2.2 Referring to the figure, the type of load is



- (a) inductive load (b) resistive load
(c) DC motor (d) capacitive load

[1994 : 1 Mark]

2.3 The output voltage of a six-pulse double star rectifier is the same as that of a three-phase half wave rectifier. (True/False).

[1994 : 1 Mark]

2.4 A three-phase AC to DC diode bridge rectifier is supplying from a three-phase, 440 V source. The rectifier supplies a purely resistive load. The average DC voltage across the load will be ___ V.

[1995 : 1 M]

2.5 A single-phase diode bridge rectifier supplies a highly inductive load. The load current can be assumed to be ripple free. The AC supply side current waveforms will be

- (a) sinusoidal (b) constant DC
(c) square (d) triangular

[1995 : 1 M]

Answers Phase Controlled Rectifiers

2.1 (4.054°) 2.2 (c) 2.3 (F) 2.1 (594.21) 2.2 (c)

Explanations Phase Controlled Rectifiers

2.1 Sol.

$$V_o = I_o R + E$$

$$\frac{V_m}{2\pi} (1 + \cos \alpha) = I_o R + E$$

$$\frac{220\sqrt{2}}{2\pi} (1 + \cos \alpha) = 100 \times 0.01 + 20$$

$$1 + \cos \alpha = 0.4241 \Rightarrow \alpha = 125.16^\circ$$

Triggering angle

$$\theta_1 = \sin^{-1} \left(\frac{E}{V_m} \right) = \sin^{-1} \left(\frac{20}{200 \times \sqrt{2}} \right) = 4.054^\circ$$

2.2 (c)

RLE load with discontinuous conduction.

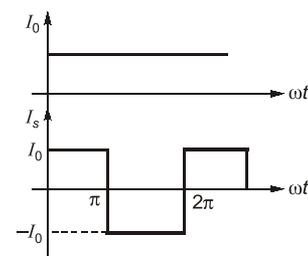
2.3 Sol.

(False)

2.1 Sol.

$$V_a = \frac{3V_{mL}}{\pi} = \frac{3 \times 440\sqrt{2}}{\pi} = 594.208 \text{ V}$$

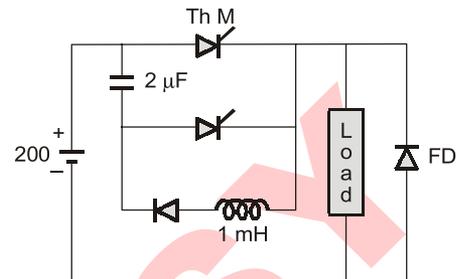
2.2 (c)



- 3.1 A chopper operating at a fixed frequency is feeding an $R-L$ load. As the duty ratio of the chopper is increased from 25% to 75%, the ripple in the load current
- remains constant.
 - decreases, reaches a minimum at 50% duty ratio and then increases.
 - increase, reaches a maximum at 50% duty ratio and then decreases.
 - keeps on increasing as the duty ratio is increased.

[1993 : 1 Mark]

- 3.2 Consider the chopper circuit shown in figure. The chopper operates at 400 Hz and 50% duty cycle. The load current remains almost ripple free at 10 A. Assuming the input voltage to be 200 V and the devices to be ideal, the circuit turn-off time available to the thyristor Th M is _____ μs .

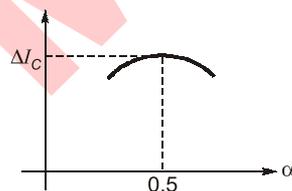


[1995 : 1 M]

- 3.3 A DC to DC transistor chopper supplied from a fixed voltage DC source feeds a fixed resistive-inductive load and a free-wheeling diode. The chopper operates at 1 kHz and 50% duty cycle. Without changing the value of the average DC current through the load, if it is desired to reduce the ripple constant of load current, the control action needed with be
- increase the chopper frequency keeping its duty cycle constant.
 - increase the chopper frequency and duty cycle in equal ratio.
 - decrease only the chopper frequency.
 - decrease only the duty cycle. [1995 : 1 M]

Answers Choppers

- 3.1 (c) 3.2 (40) 3.3 (a)

Explanations Choppers**3.1 (c)****3.2 Sol.**

$$t_c = \frac{CV_s}{I} = \frac{2 \times 10^{-6} \times 200}{10} = 40 \mu\text{s}$$

3.3 (a)

$$\Delta I_c = \frac{V_s}{4fL}$$

■■■■

- 4.1** When a line commutated converter operates in the inverter mode?
 (a) It draws both real and reactive power from the AC supply.
 (b) It delivers both real and reactive power to the AC supply.
 (c) It delivers real power to the AC supply.
 (d) It draws reactive power from the AC supply.
[1993 : 1 Mark]
- 4.2** A line-commutated inverter changes DC voltage to AC voltage. (True/False)
[1994 : 1 Mark]
- 4.3** A single-phase inverter with square wave output voltage will have in its output waveform a fifth harmonic component equal to _____ percentage of the fundamental.
[1995 : 1 M]
- 4.4** An inverter capable of supplying a balanced three-phase variable voltage variable frequency output, is feeding a three-phase induction motor rated for 50 Hz and 440 V. The stator winding resistance of the motor are negligibly small during starting. The current inrush can be avoided without sacrificing the starting torque by suitably applying.
 (a) Low voltage as rated frequency.
 (b) Low voltage keeping the v/f ratio constant.
 (c) Rated voltage at low frequency.
 (d) Rated voltage at rated frequency.
[1995 : 1 M]

■■■■

Answers Inverters

4.1 (c) 4.2 (T) 4.3 (20) 4.4 (b)

Explanations Inverters**4.2 Sol.**

(True).

4.3 Sol.

For a square wave, fourier series can be given as:

$$V_o = \sum_{n=1,3,5}^{\infty} \frac{4V_s}{n\pi} \sin n\omega t$$

For fundamental component

$$V_1 = \frac{4V_s}{\pi \times \sqrt{2}} \quad \dots(i)$$

For fifth harmonics

$$V_5 = \frac{4V_s}{5\pi \times \sqrt{2}} \quad \dots(ii)$$

$$\text{Percentage} = \frac{4V_s/5\sqrt{2}\pi}{4V_s/\sqrt{2}\pi} \times 100 = \frac{1}{5} \times 100 = 20\%$$

■■■■

5.1 Match the items on the List-I with List-II.

- | List-I | List-II |
|------------------------|----------------------|
| A. Commutation | P. Resistive load |
| B. V-Curves | Q. Inductive load |
| C. Free wheeling diode | R. Capacitance load |
| D. Overlap | S. Inter pole |
| | T. Source inductance |
| | U. Synchronous motor |
- [1994 : 1 Mark]

5.2 Thyristor circuits that directly convert polyphase ac voltages from one frequency to another frequency are called _____. [1994 : 1 Mark]

Answers Miscellaneous

5.1 (Sol.) 5.2 (Sol.)

Explanations Miscellaneous

5.1 Sol.

- A — S
 B — U
 C — Q
 D — T

5.2 Sol.

Thyristor circuits that directly convert polyphase ac voltages from one frequency to another frequency are called *cycloconverters*.

■■■■

Electromagnetic Theory

UNIT X

CONTENTS

1. Electrostatic Fields 70
2. Magnetostatic Fields 71

MADE

1.1 An electrostatic potential is given by $\phi = 2x\sqrt{y}$ volts in the rectangular co-ordinate system. The magnitude of the electric field at $x = 1$ m, $y = 1$ m is _____ V/m. [1992 : 1 Mark]

1.2 Which of the following equations represents the Gauss' law in a homogenous isotropic medium?

(a) $\iint \vec{D} \cdot d\vec{S} = \iiint \rho dv$ (b) $\nabla \times \vec{H} = \vec{D}$

(c) $\nabla \cdot \vec{J} + \rho = 0$ (d) $\nabla \cdot \vec{E} = \frac{\rho}{\epsilon}$ [1992 : 1 Mark]

1.3 In electrostatic field, $\nabla \times \vec{E} \equiv 0$ (True/False).

[1994 : 1 Mark]

Answers Electrostatic Fields

1.1 (2.24) 1.2 (a) 1.3 (T)

Explanations Electrostatic Fields

1.1 Sol.

Electrostatic potential, $\phi = 2x\sqrt{y}$

$$\therefore \vec{E} = -\text{grad}(\phi) = -\nabla\phi$$

$$\therefore \vec{E} = -\left[\hat{a}_x \frac{\partial}{\partial x}(2x\sqrt{y}) + \hat{a}_y \frac{\partial}{\partial y}(2x\sqrt{y})\right]$$

$$\vec{E} = -\hat{a}_x 2\sqrt{y} - \hat{a}_y \frac{x}{\sqrt{y}}$$

Now, at $x = 1$ m and $y = 1$ m

$$\vec{E} = -2\hat{a}_x - \hat{a}_y$$

Magnitude of \vec{E}

$$|\vec{E}| = \sqrt{2^2 + 1^2} = \sqrt{5} = 2.24 \text{ V/m}$$

1.2 (a)

Gauss Law: The electric flux passing through any closed surface is equal to the total charge in the volume enclosed by the surface i.e. $\iint \vec{D} \cdot d\vec{S} = \iiint \rho_v dV$.

1.3 Sol. (True)

By stroke's theorem,

$$\int_s (\nabla \times \vec{E}) \cdot d\vec{s} = \oint_c \vec{E} \cdot d\vec{l}$$

which represents the potential difference around a closed path, C which is zero in electrostatic field.

Hence, $\nabla \times \vec{E} = 0$ i.e. electromagnetic fields are conservative in nature.



2.1 The line integral of the vector potential A around the boundary of a surface S represents

- (a) flux through the surface S
- (b) flux density in the surface S
- (c) magnetic density
- (d) current density

[1993 : 1 Mark]

2.2 Static magnetic fields induce currents in closed conducting loops. (True/False)

[1994 : 1 Mark]

Answers Magnetostatic Fields

2.1 (a) 2.2 (F)

Explanations Magnetostatic Fields

2.1 (a)

Using Stoke's theorem,

$$\oint \vec{A} \cdot d\vec{L} = \int_s (\nabla \times \vec{A}) \cdot d\vec{s}$$

$\therefore \vec{A}$ is vector magnetic potential

$$\Rightarrow \nabla \times \vec{A} = \text{curl}(\vec{A})$$

= Magnetic flux density \vec{B}

$$\Rightarrow \int_s (\nabla \times \vec{A}) \cdot d\vec{s} = \int_s \vec{B} \cdot d\vec{s}$$

= Flux through the surface S .

2.2 Sol. (False)

According to Faraday's law: induced voltage $\propto \frac{d\phi}{dt}$ i.e. only time varying fields induce voltage and hence responsible for production of induced currents in closed loops.

■■■■

Engineering Mathematics

UNIT XI

CONTENTS

1. Linear Algebra 73
2. Laplace Transform 75

MADE

1.1 A 5×7 matrix has all its entries equal to -1 . Then the rank of a matrix is

- (a) 7 (b) 5
(c) 1 (d) 0

[1994 : 1 Mark]

1.2 The eigen values of the matrix $\begin{bmatrix} a & 1 \\ a & 1 \end{bmatrix}$ are

- (a) $(a+1), 0$ (b) $a, 0$
(c) $(a-1), 0$ (d) $0, 0$

[1994 : 1 Mark]

1.3 The number of linearly independent solutions of the system of equations

$$\begin{bmatrix} 1 & 0 & 2 \\ 1 & -1 & 0 \\ 2 & -2 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = 0 \text{ is equal to}$$

- (a) 1 (b) 2
(c) 3 (d) 0

[1994 : 2 Marks]

1.4 The inverse of the matrix, $S = \begin{bmatrix} 1 & -1 & 0 \\ 1 & 1 & 1 \\ 0 & 0 & 1 \end{bmatrix}$ is

(a) $\begin{bmatrix} 1 & 0 & 1 \\ 0 & 0 & 0 \\ 0 & 1 & 1 \end{bmatrix}$ (b) $\begin{bmatrix} 0 & 1 & 1 \\ -1 & -1 & 1 \\ 1 & 0 & 1 \end{bmatrix}$

(c) $\begin{bmatrix} 2 & 2 & -2 \\ -2 & 2 & -2 \\ 0 & 2 & 2 \end{bmatrix}$ (d) $\begin{bmatrix} \frac{1}{2} & \frac{1}{2} & -\frac{1}{2} \\ \frac{1}{2} & \frac{1}{2} & \frac{1}{2} \\ 0 & 0 & 1 \end{bmatrix}$

[1995 : 2 M]

1.5 Given the matrix, $A = \begin{bmatrix} 0 & 1 & 0 \\ 0 & 0 & 1 \\ -6 & -11 & -6 \end{bmatrix}$. Its eigen values are

[1995 : 2 M]

■■■■

Answers Linear Algebra

1.1 (c) 1.2 (a) 1.3 (b) 1.4 (d) 1.5 $(-1, -2, -3)$

Explanations Linear Algebra

1.1 (c)

$$A = \begin{bmatrix} -1 & -1 & -1 & -1 & -1 & -1 & -1 \\ -1 & -1 & -1 & -1 & -1 & -1 & -1 \\ -1 & -1 & -1 & -1 & -1 & -1 & -1 \\ -1 & -1 & -1 & -1 & -1 & -1 & -1 \\ -1 & -1 & -1 & -1 & -1 & -1 & -1 \end{bmatrix}$$

$$\simeq \begin{bmatrix} -1 & -1 & -1 & -1 & -1 & -1 & -1 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 & 0 & 0 & 0 \end{bmatrix}$$

$R_2 - R_1, R_3 - R_1, R_4 - R_1, R_5 - R_1$
number of non-zero rows = 1
 \therefore rank = 1

1.2 (a)

Ch. equation is $|A - \lambda I| = 0$

$$\begin{vmatrix} a-\lambda & 1 \\ a & 1-\lambda \end{vmatrix} = 0$$

$$(a-\lambda)(1-\lambda) - a = 0$$

$$a - a\lambda - \lambda + \lambda^2 - a = 0$$

$$\lambda^2 - (a+1)\lambda = 0$$

$$\lambda = 0, \lambda = a+1$$

1.3 (b)

$$\begin{bmatrix} 1 & 0 & 2 \\ 1 & -1 & 0 \\ 2 & -2 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$R_2 - R_1, R_3 - 2R_1$$

$$\begin{bmatrix} 1 & 0 & 2 \\ 0 & -1 & -2 \\ 0 & -2 & -4 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

$$R_3 - 2R_2$$

$$\begin{bmatrix} 1 & 0 & 2 \\ 0 & -1 & -2 \\ 0 & 0 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \\ 0 \end{bmatrix}$$

Rank = 2 number of variables = 3

Nullity = number of linearly independent solutions = 2

1.4 (d)

$$|S| = 1(1-0) + 1(1-0) = 1 + 1 = 2$$

$$\text{Adj } S = \begin{bmatrix} 1 & 1 & -1 \\ -1 & 1 & -1 \\ 0 & 0 & 2 \end{bmatrix}$$

$$S^{-1} = \frac{\text{Adj } S}{|S|} = \begin{bmatrix} 1/2 & 1/2 & -1/2 \\ -1/2 & 1/2 & -1/2 \\ 0 & 0 & 1 \end{bmatrix}$$

1.5 (-1, -2, -3)The ch. equation is $|A - \lambda I| = 0$

$$\begin{vmatrix} 0-\lambda & 1 & 0 \\ 0 & 0-\lambda & 1 \\ -6 & -11 & -6-\lambda \end{vmatrix} = 0$$

$$(-\lambda) [6\lambda + \lambda^2 + 11] - 1(0 + 6) = 0$$

$$-6\lambda^2 - \lambda^3 - 11\lambda - 6 = 0$$

$$\lambda^3 + 6\lambda^2 + 11\lambda + 6 = 0$$

$$\lambda = -1, -2, -3$$

■■■■

2.1 The Laplace transform of $f(t)$ is $F(s)$.

Given $F(s) = \frac{\omega}{s^2 + \omega^2}$, the final value of $f(t)$ is ___

- (a) initially (b) zero
(c) one (d) none [1995 : 1 M]

■■■■

Answers Linear Algebra

2.1 (d)

Explanations Linear Algebra

2.1 (d)

$$F(s) = \frac{\omega}{s^2 + \omega^2}$$

$$\therefore f(t) = \sin \omega t$$

$$\lim_{t \rightarrow \infty} f(t) = \lim_{t \rightarrow \infty} \sin \omega t = \text{Lies between } -1 \text{ and } 1$$

■■■■