

POSTAL Book Package

2021

Mechanical Engineering

Objective Practice Sets

Renewable Sources of Energy

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Solar Thermal Energy Collection

- [illegible]

- Q.23** The optimum inclination of a FPC for summer condition is:
 (a) ϕ (latitude) (b) $\phi - 15$
 (c) $\phi + 15$ (d) None of the above
- Q.24** The optimum inclination of a FPC for winter condition is _____.
 (a) ϕ (latitude) (b) $\phi + 15$
 (c) $\phi - 15$ (d) None of the above
- Q.25** The annual optimum inclination of a FPC is:
 (a) ϕ (latitude) (b) $\phi + 15$
 (c) $\phi - 15$ (d) None of the above
- Q.26** A cylindrical parabolic concentrator of 3 m width and 12 m length is used in power plant. If the inside and outside diameter of the absorber tube are 60 mm and 65 mm respectively, find out concentration ratio of the collector.
 (a) 15.6 (b) 14.4
 (c) 58.4 (d) 63.3
- Q.27** For a parabolic collector of length 2 m, the angle of acceptance is 18° . Find out the concentration ratio.
 (a) 6.4 (b) 3.2
 (c) 12.8 (d) 1.6
- Q.28** The optical efficiency of concentration (solar thermal energy concentrator) is:
 (a) more than the thermal efficiency
 (b) equal to thermal efficiency
 (c) less than the thermal efficiency
 (d) can't be compared
- Q.29** The concentration ratio (c) is defined as
 (a) Area of absorber plate/area of the aperture
 (b) Area of aperture/2
 (c) Area of absorber plate / $\sin \theta$
 (d) Area of aperture to the area of absorber plate



Answers Solar Thermal Energy Collection

1. (b) 2. (c) 3. (d) 4. (b) 5. (c) 6. (c) 7. (a) 8. (c) 9. (c)
 10. (c) 11. (a) 12. (b) 13. (a) 14. (c) 15. (d) 16. (a) 17. (c) 18. (a)
 19. (a) 20. (a) 21. (d) 22. (d) 23. (b) 24. (b) 25. (a) 26. (b) 27. (a)
 28. (a) 29. (d)

Explanations Solar Thermal Energy Collection

4. (b)

Tilt factor for reflected radiation

$$r_r = \rho \left(\frac{1 - \cos \beta}{2} \right) = \rho \left(\frac{1 - \cos 0}{2} \right) = 0$$

Tilt factor for beam radiations

$$= \frac{\cos \theta}{\cos \theta_z}, \text{ For horizontal surface}$$

$$= \theta = \theta_z$$

Hence $r_b = 1$

5. (c)

Tilt factor for diffused radiation (r_d)

$$r_d = \frac{1 + \cos \beta}{2}$$

β varies from 0° to 90°

$$(r_d)_{0^\circ} = \frac{1 + \cos 0^\circ}{2} = 1$$

$$(r_d)_{90^\circ} = \frac{1 + \cos 90^\circ}{2} = 0.5$$

$$\text{variation} = 1 - 0.5 = 0.5$$

6. (c)

Global radiation falling as collector

$$(I_g) = 2400 \text{ kJ/m}^2 - \text{hr}$$

Diffused radiation

$$(I_d) = \frac{20 \times 2400}{100} = 480 \text{ kJ/m}^2\text{hr}$$

Beam radiations

$$(I_b) = I_g - I_d = 2400 - 480 \\ = 1920 \text{ kJ/m}^2 - \text{hr}$$

Total flux falling (I_T)

$$I_T = I_b r_b + I_d r_d + (I_b + I_d) r_r$$

Now

$$r_b = 0.95$$

$$r_d = \frac{1 + \cos \beta}{2} = 0.933$$

$$r_r = \rho \left(\frac{1 - \cos \beta}{2} \right) \\ = 0.18 \left[\frac{1 - \cos 30}{2} \right] = 0.0121$$

$$\therefore I_T = 1920 \times 0.95 + 480 \times 0.933 \\ + 0.0121 \times 2400 \\ = 2300.78 \text{ kJ/m}^2 - \text{hr}$$

7. (a)

Total flux falling are given by (I_T)

$$I_T = I_b r_b + I_d r_d + (I_b + I_d) r_r$$

For horizontal surface, $\beta = 0^\circ$ and $\theta = \theta_z$

$$\therefore r_b = \frac{\cos \theta}{\cos \theta_z} = 1$$

$$r_d = \frac{1 + \cos \beta}{2} = \frac{1 + \cos 0}{2} = 1$$

$$r_r = \rho \left(\frac{1 - \cos \beta}{2} \right) = \left(\frac{1 - \cos 0}{2} \right) \rho = 0$$

$$I_T = I_b \times 1 + I_d \times 1 + I_g \times 0$$

$$I_T = I_b + I_d$$

$$I_T = I_g = 1800 \text{ kJ/m}^2 - \text{hr}$$

Flux absorbed by the collector systems is given by:

$$S = (\tau \alpha) I_T = 0.81 \times 1800$$

$$S = 1458 \text{ kJ/m}^2 - \text{hr}$$

8. (c)

Collector efficiency is given by:

$$\eta_c = \frac{q_u}{A_c I_T}$$

Useful heat gain (q_u) = Total heat gain – heat losses

$$q_u = q_T - q_l$$

As $q_l = 0$

$$\therefore q_u = q_T$$

Total heat gain $q_T = (\tau \alpha) I_T \times A_p$

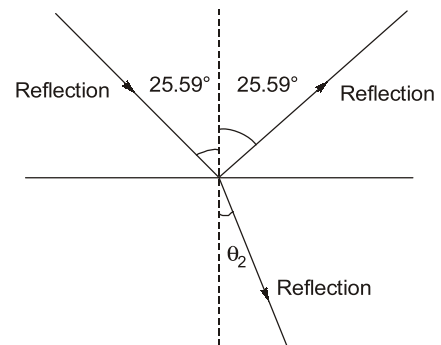
where I_T is total flux falling on the collector

A_p is area of absorber plate

A_c is area of collector system

$$\therefore \eta_c = \frac{(\tau \alpha) A_p I_T}{A_c I_T} \\ = \frac{(0.93) \times 2.9 \times 1.95}{6} = 0.8765 \\ = 87.65\%$$

9. (c)



Refraction angle can be determined with Snell's law i.e.

$$\frac{\sin \theta}{\sin \theta_2} = \frac{n_1}{n_2} \\ \Rightarrow \frac{\sin 25.59^\circ}{\sin \theta_2} = 1.48 \\ \Rightarrow \theta_2 = 16.97^\circ$$

10. (c)

Incidence angle (θ) = 25°

Beam refraction angle can be obtained from Snell's

law i.e. $\frac{\sin \theta}{\sin \theta_2} = \frac{n_1}{n_2}$

$$\Rightarrow \frac{\sin 25}{\sin \theta_2} = 1.42$$

$$\Rightarrow \theta_2 = 17.31^\circ$$

Now reflectivity of the system is given by

$$\rho_I = \frac{\sin^2(\theta_2 - \theta)}{\sin^2(\theta_2 + \theta)}$$

$$\rho_{II} = \frac{\tan^2(\theta_2 - \theta)}{\tan^2(\theta_2 + \theta)}$$

$$\therefore \rho_I = \frac{\sin^2(25 - 17.31)}{\sin^2(25 + 17.31)} = 0.04$$

17. (c)

Bond resistance is given by:

$$R_b = \frac{k_b \times b}{r} = \frac{250 \times 25}{0.5} = 25000$$

Bond conductance (C_b)

$$C_b = \frac{1}{R_b} = \frac{1}{25000} = 4 \times 10^{-5} \text{ W/m}^\circ\text{C}$$

18. (a)

Thermal resistance offered by tubes is given by:

$$\begin{aligned} \frac{1}{h_{f1} \pi D_i} &= \frac{1}{200 \times \pi \times 10 \times 10^{-3}} \\ &= 0.159 \text{ (W/m}^\circ\text{C)}^{-1} \end{aligned}$$

26. (b)

Concentration ratio

$$= \frac{W - D_0}{\pi D_0} = \frac{3000 - 65}{\pi \times 65} = 14.37$$

27. (a)

Concentration ratio (CR)

$$= \frac{1}{\sin \theta_{\max}}$$

$$\text{Now } \theta_{\max} = \frac{\text{angle of acceptance}}{2}$$

$$= \frac{18}{2} = 9^\circ$$

$$\therefore CR = \frac{1}{\sin 9^\circ} = 6.39$$

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